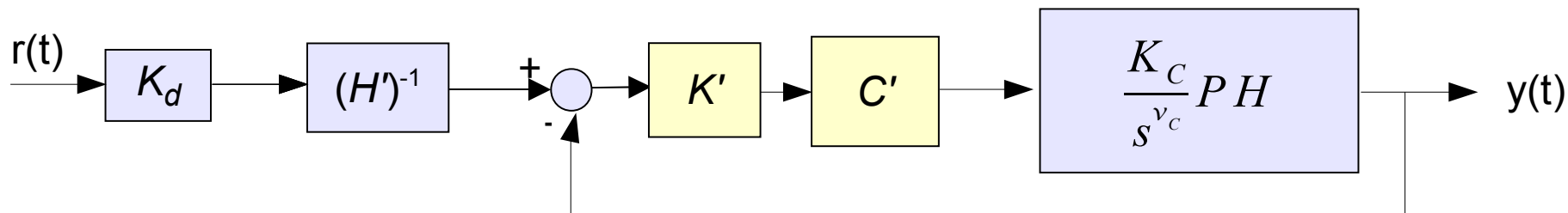


# Sintesi mediante luogo delle radici

- Specifiche del transitorio nel piano complesso
- Criteri generali per la sintesi
- Esempi di sintesi

## Specifiche del transitorio nel piano complesso



Il blocco  $K'$  può assumere valori inferiori a 1 solo e soltanto se la presenza di un adeguato numero di poli nell'origine nel controllore e/o nel processo garantisce il rispetto delle specifiche sul comportamento a regime a prescindere dal valore del guadagno

$$B_3 \approx \bar{B}_3$$

$$s \leq \bar{s}$$

$$M_r \leq \bar{M}_r$$

$$t_s \leq \bar{t}_s$$

$$t_s \leq \bar{t}_s \Leftrightarrow B_3 \geq \bar{B}_3$$

$$t_a \leq \bar{t}_a$$

$$t_{a_{\varepsilon^o/o}} \leq \bar{t}_a \Leftrightarrow B_3 \geq \bar{B}_3$$

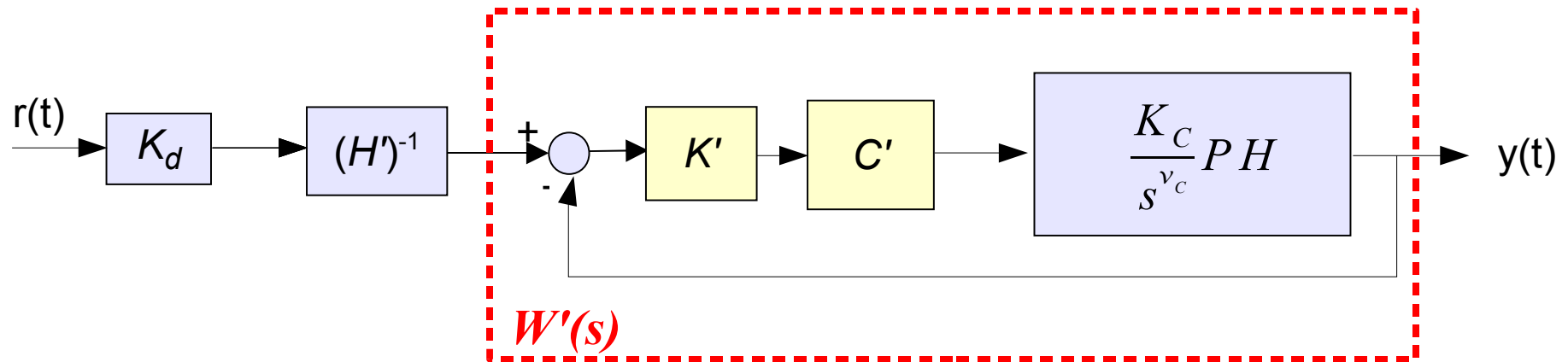
$$B_3 \approx \bar{B}_3 \Leftrightarrow \omega_n \approx \bar{\omega}_n$$

$$M_r \leq \bar{M}_r; \quad s \leq \bar{s} \Leftrightarrow \xi \geq \bar{\xi}$$

$$t_s \leq \bar{t}_s \Rightarrow \omega_n \geq \bar{\omega}_n$$

$$t_{a_{\varepsilon^o/o}} \leq \bar{t}_a \Rightarrow \tau_{eq} = \frac{1}{\xi \omega_n} \leq \bar{\tau}$$

## Specifiche del transitorio nel piano complesso



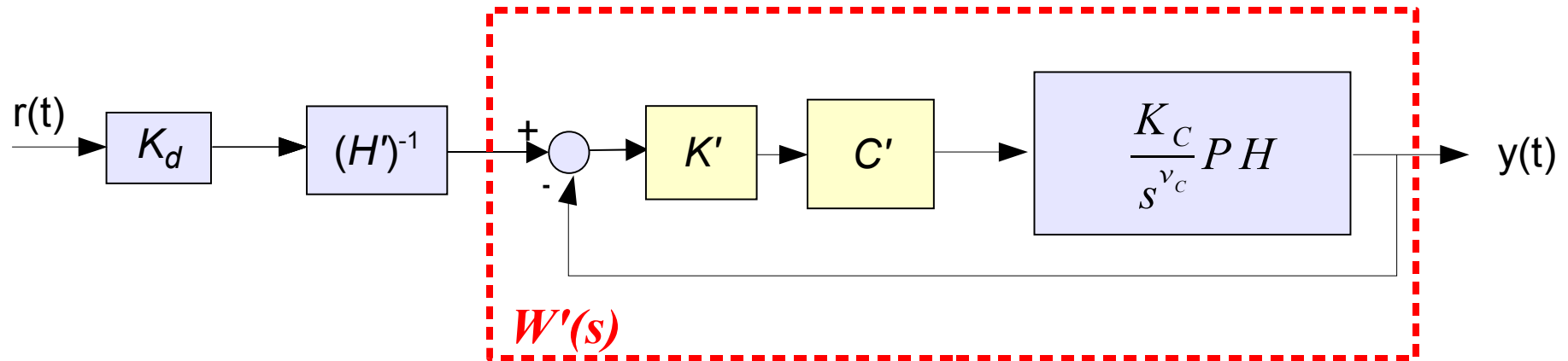
$$W'(s) = \frac{F'(s)}{1 + F'(s)} = \frac{N_{F'}(s)}{D_{F'}(s) + K' N_{F'}(s)}$$

$$F'(s) = K' C'(s) \frac{K_c}{s^{v_c}} P(s) H(s)$$

I poli di  $W'$  possono essere valutati con il metodo del luogo delle radici

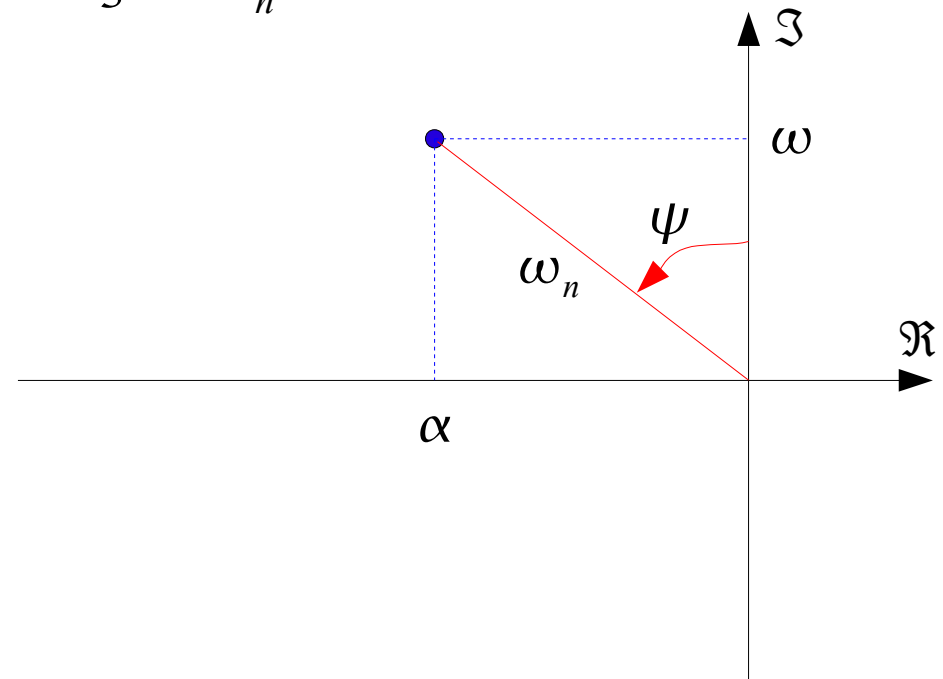
Inserendo poli e zeri in  $C'$  il luogo delle radici può essere modificato in modo che sia possibile definire valori di  $K'$  per cui i poli a ciclo chiuso giacciono in una specifica zona del piano complesso

## Specifiche del transitorio nel piano complesso



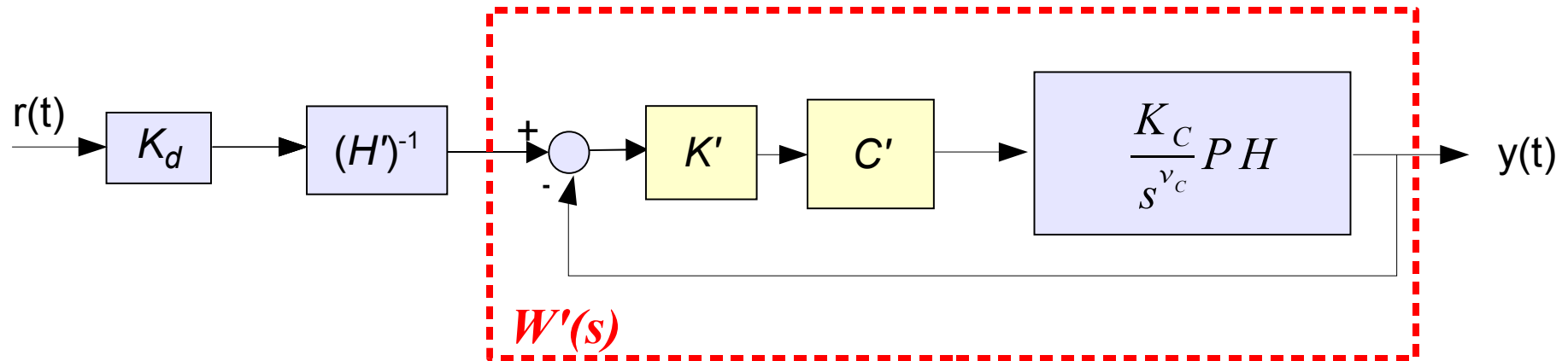
$$p_{i,i+1}^{W'} = \alpha \pm j\omega = -\xi\omega_n \pm j\omega_n\sqrt{1-\xi^2} = \omega_n e^{\pm j(\frac{\pi}{2} + \psi)}$$

$$\xi = \sin(\psi)$$



I poli di  $W'$  possono essere valutati con il metodo del luogo delle radici

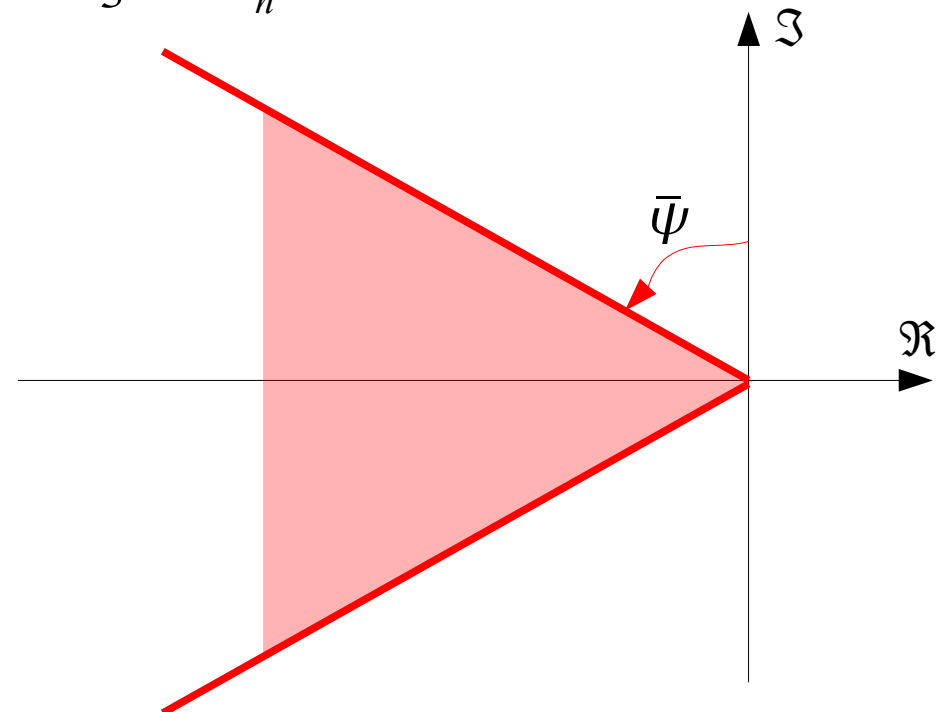
## Specifiche del transitorio nel piano complesso



$$p_{i,i+1}^{W'} = \alpha \pm j\omega = -\xi\omega_n \pm j\omega_n \sqrt{1-\xi^2} = \omega_n e^{\pm j(\frac{\pi}{2} + \psi)}$$

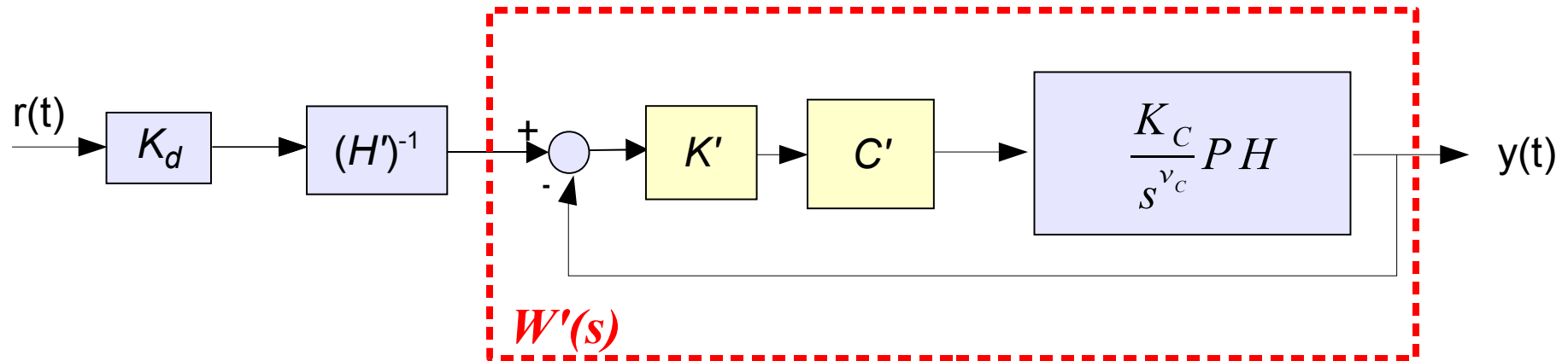
$$\xi = \sin(\psi)$$

$$\xi \geq \bar{\xi} \Leftrightarrow \psi \geq \bar{\psi}$$



I poli di  $W'$  possono essere valutati con il metodo del luogo delle radici

## Specifiche del transitorio nel piano complesso

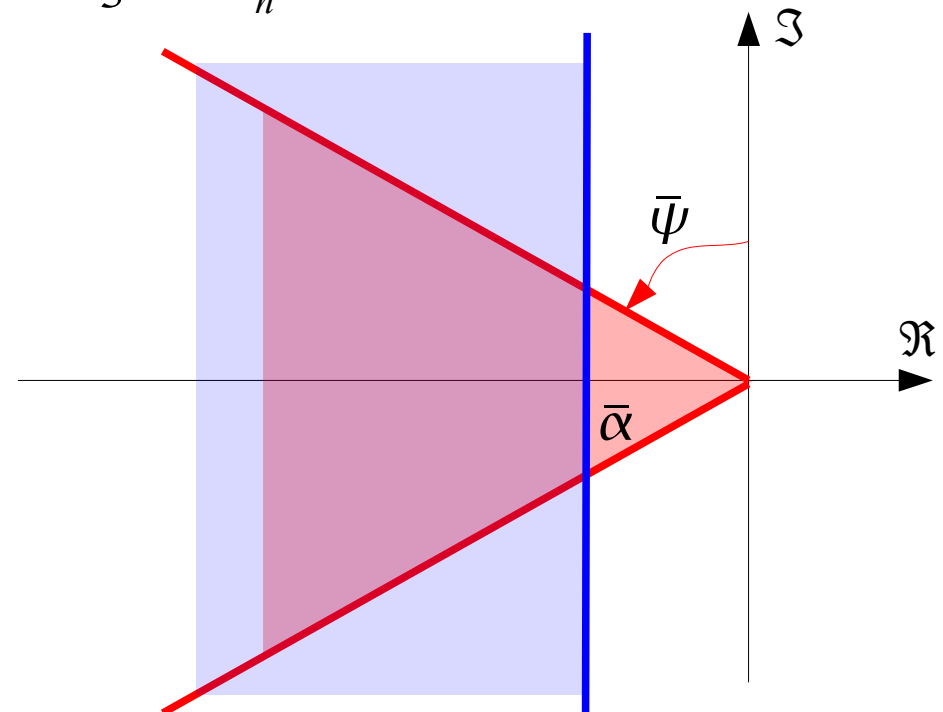


$$p_{i,i+1}^{W'} = \alpha \pm j\omega = -\xi\omega_n \pm j\omega_n \sqrt{1-\xi^2} = \omega_n e^{\pm j(\frac{\pi}{2} + \psi)}$$

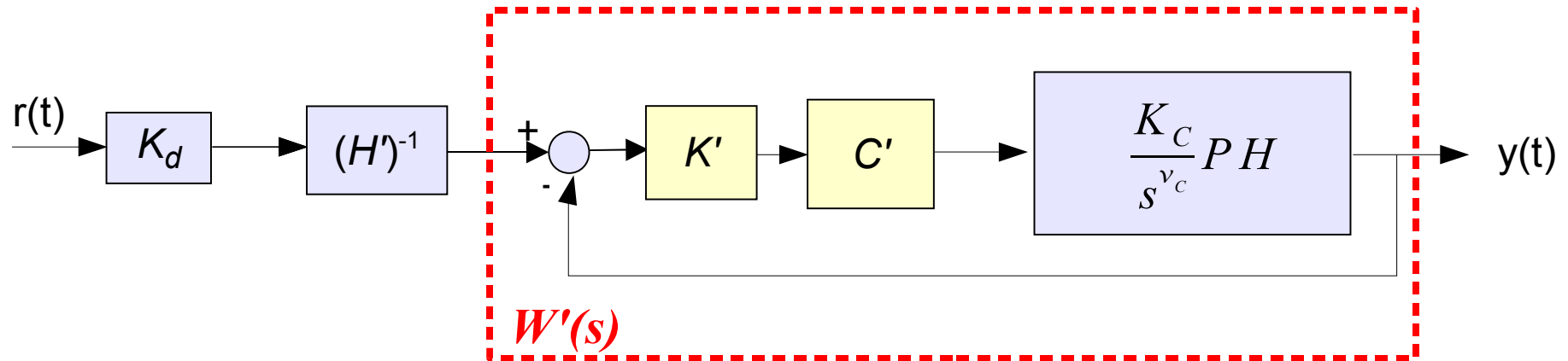
$$\xi = \sin(\psi)$$

$$\xi \geq \bar{\xi} \Leftrightarrow \psi \geq \bar{\psi}$$

$$\xi\omega_n \leq \frac{1}{\bar{\tau}} = \bar{\alpha} \Leftrightarrow \alpha \leq \bar{\alpha}$$



## Specifiche del transitorio nel piano complesso



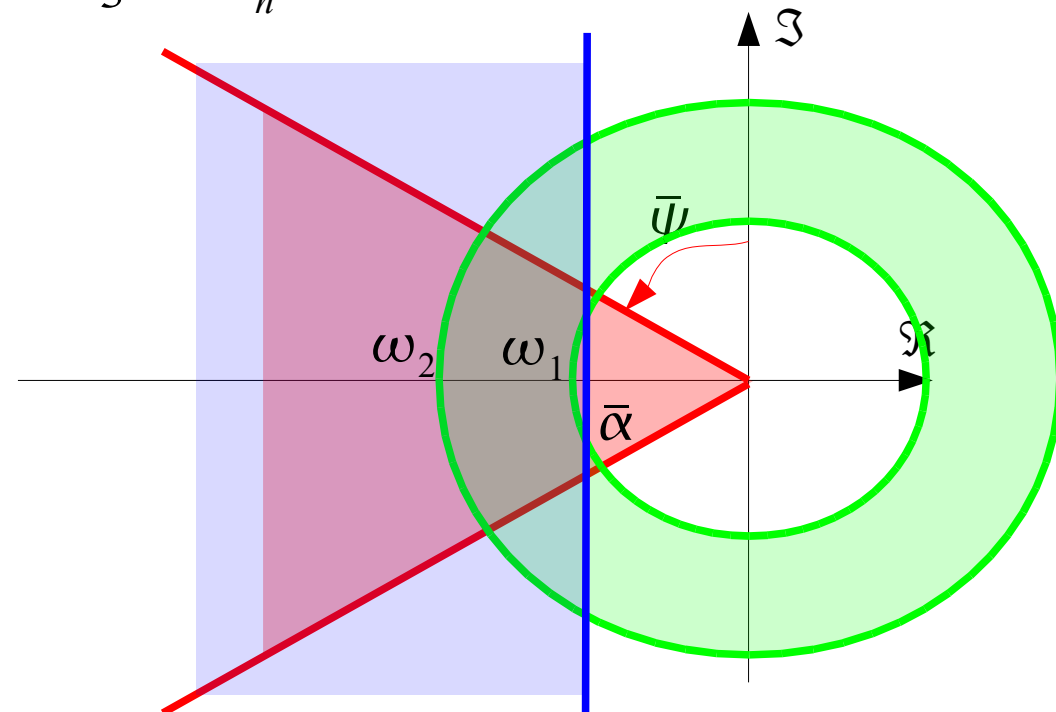
$$p_{i,i+1}^{W'} = \alpha \pm j\omega = -\xi\omega_n \pm j\omega_n \sqrt{1-\xi^2} = \omega_n e^{\pm j(\frac{\pi}{2} + \psi)}$$

$$\xi = \sin(\psi)$$

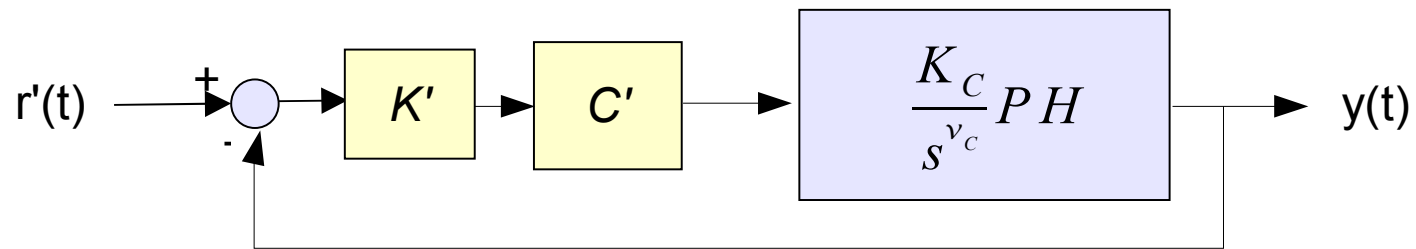
$$\xi \geq \bar{\xi} \Leftrightarrow \psi \geq \bar{\psi}$$

$$\xi\omega_n \leq \frac{1}{\bar{\tau}} = \bar{\alpha} \Leftrightarrow \alpha \leq \bar{\alpha}$$

$$\omega_n \approx \bar{\omega}_n \Leftrightarrow \omega_1 \leq \omega_n \leq \omega_2$$



## Criteri generali per la sintesi



NON cancellare poli e zeri a parte reale positiva

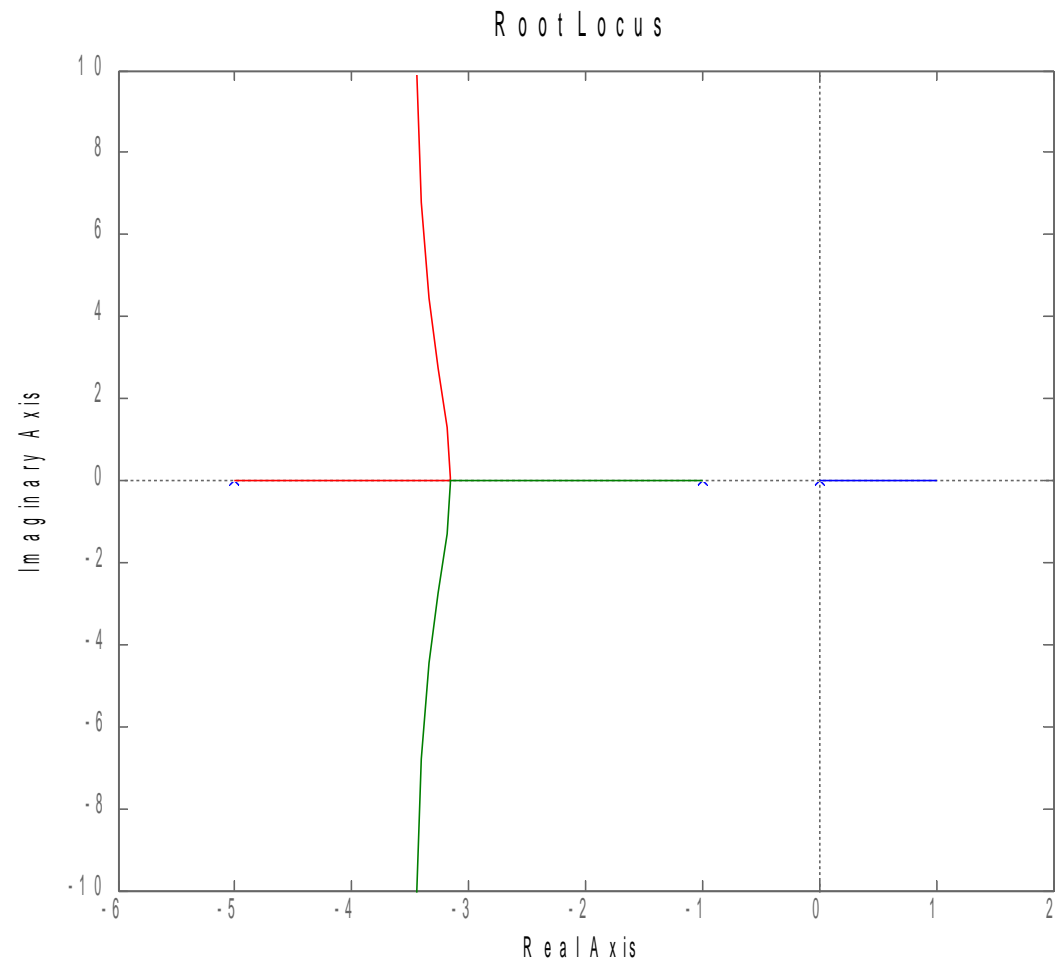
$$H = 1$$

$$K_C = 1$$

$$v_C = 1$$

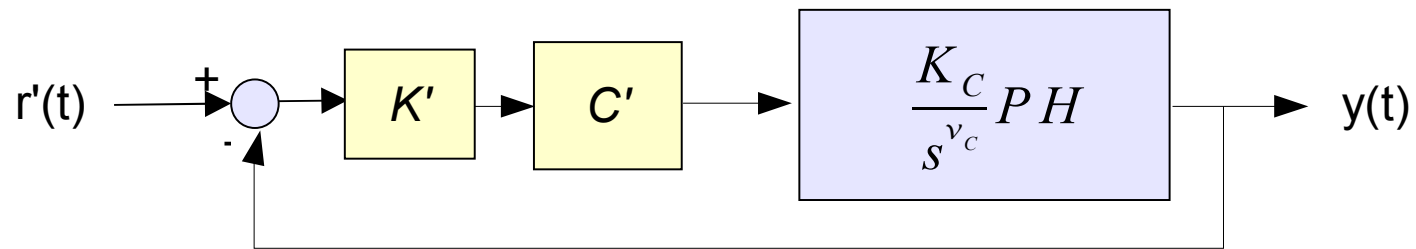
$$P(s) = \frac{s-1}{(s+1)(s+5)}$$

La parte del semiasse reale a destra del polo nell'origine appartiene al luogo





## Criteri generali per la sintesi



NON cancellare poli e zeri a parte reale positiva

$$H = -1$$

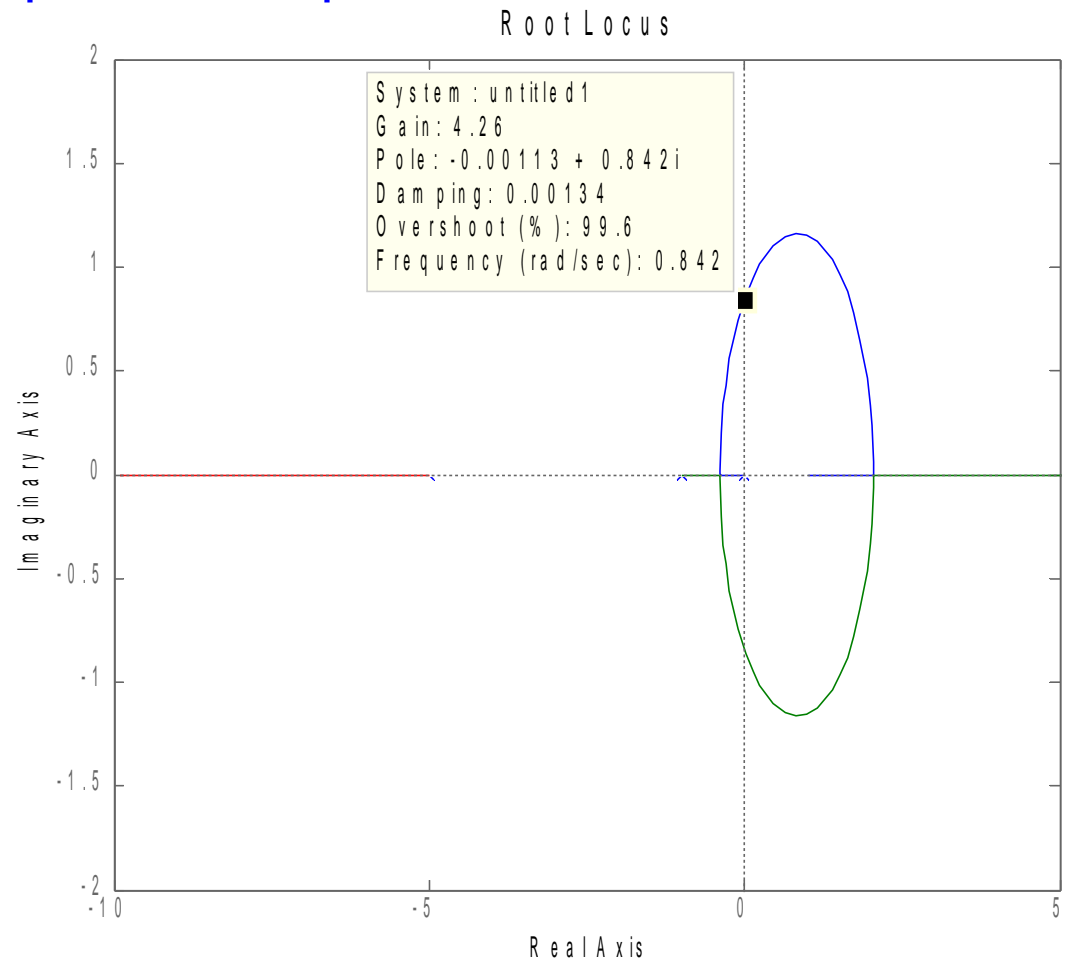
$$K_C = 1$$

$$v_C = 1$$

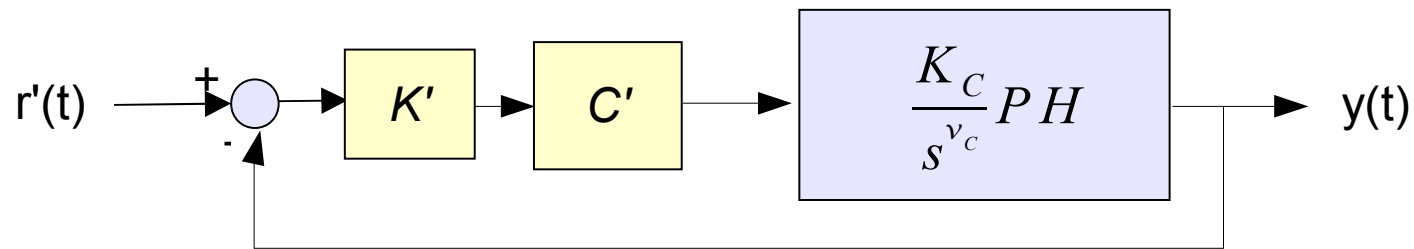
$$P(s) = \frac{s-1}{(s+1)(s+5)}$$

Realizzare un sistema a retroazione positiva

$$K' \leq 4,26$$



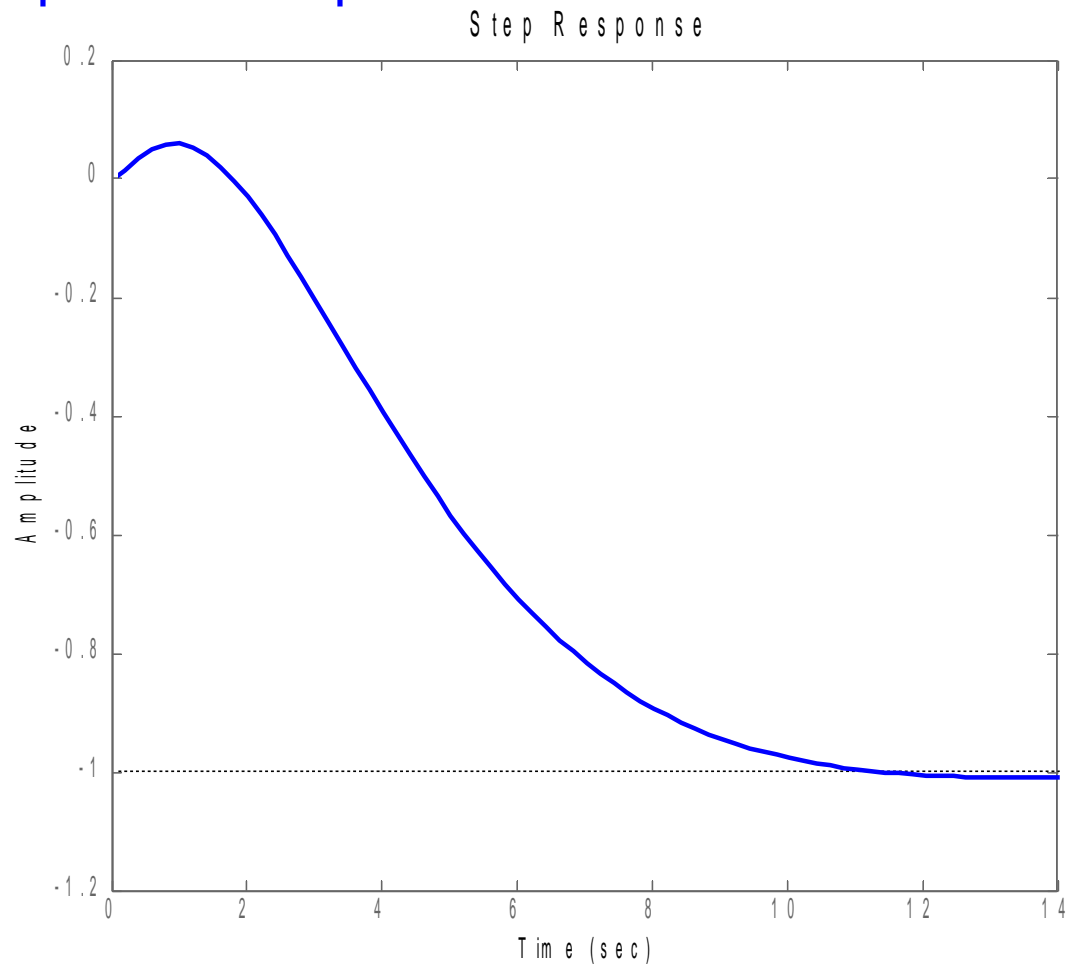
## Criteri generali per la sintesi



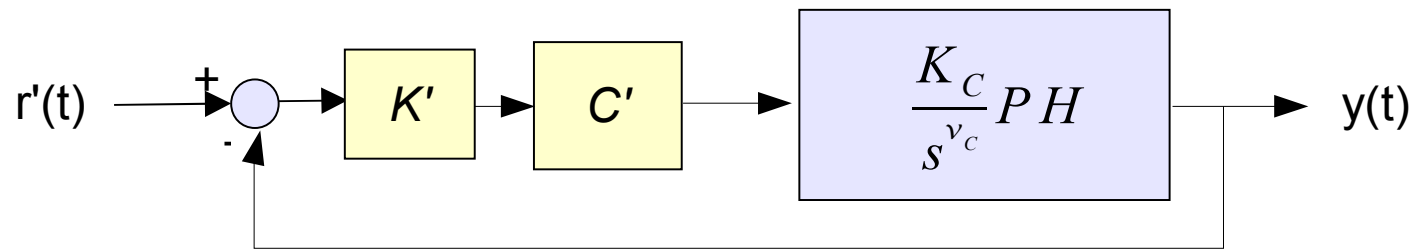
NON cancellare poli e zeri a parte reale positiva

$$\begin{aligned} H &= -1 \\ K_C &= 1 \\ v_C &= 1 \\ P(s) &= \frac{s-1}{(s+1)(s+5)} \end{aligned}$$

A causa del guadagno negativo di P si ha guadagno negativo a ciclo chiuso



## Criteri generali per la sintesi



NON cancellare poli e zeri a parte reale positiva

$$H=1$$

$$K_C=1$$

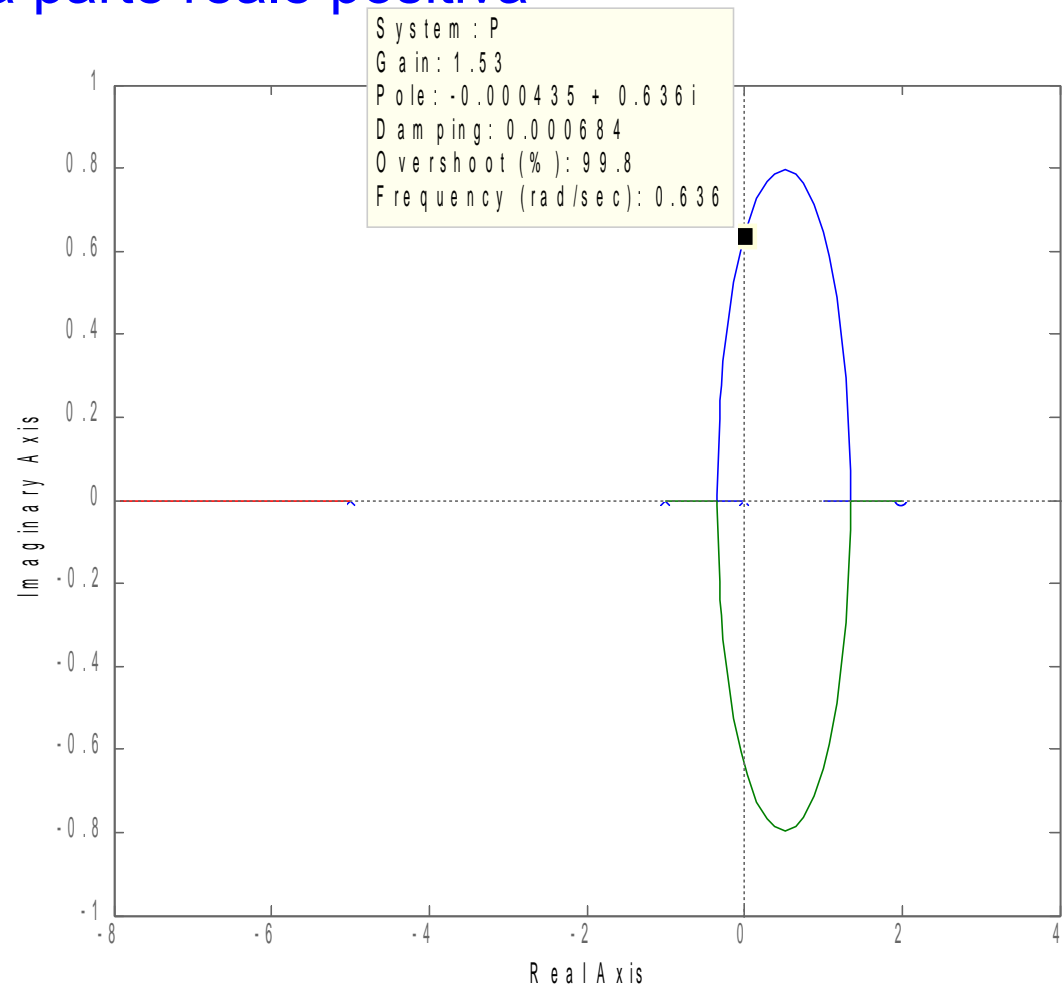
$$v_C=1$$

$$P(s)=\frac{s-1}{(s+1)(s+5)}$$

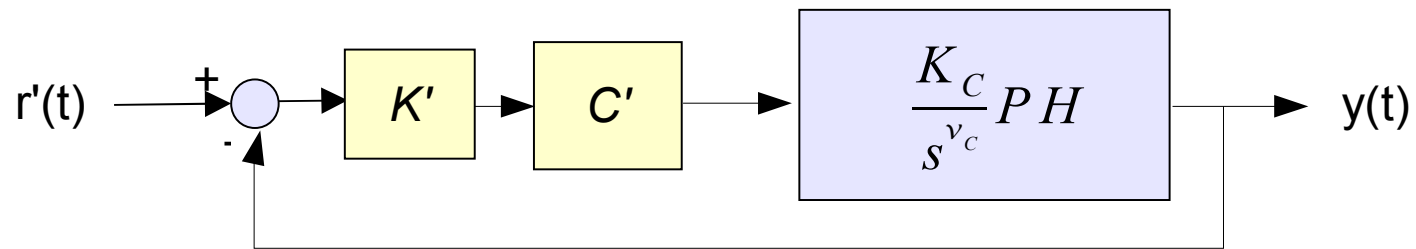
Inserire uno zero a parte reale positiva nel controllore

$$C(s)=K' \frac{s-2}{s}$$

$$K' \leq 1,53$$



## Criteri generali per la sintesi



NON cancellare poli e zeri a parte reale positiva

$$H = 1$$

$$K_C = 1$$

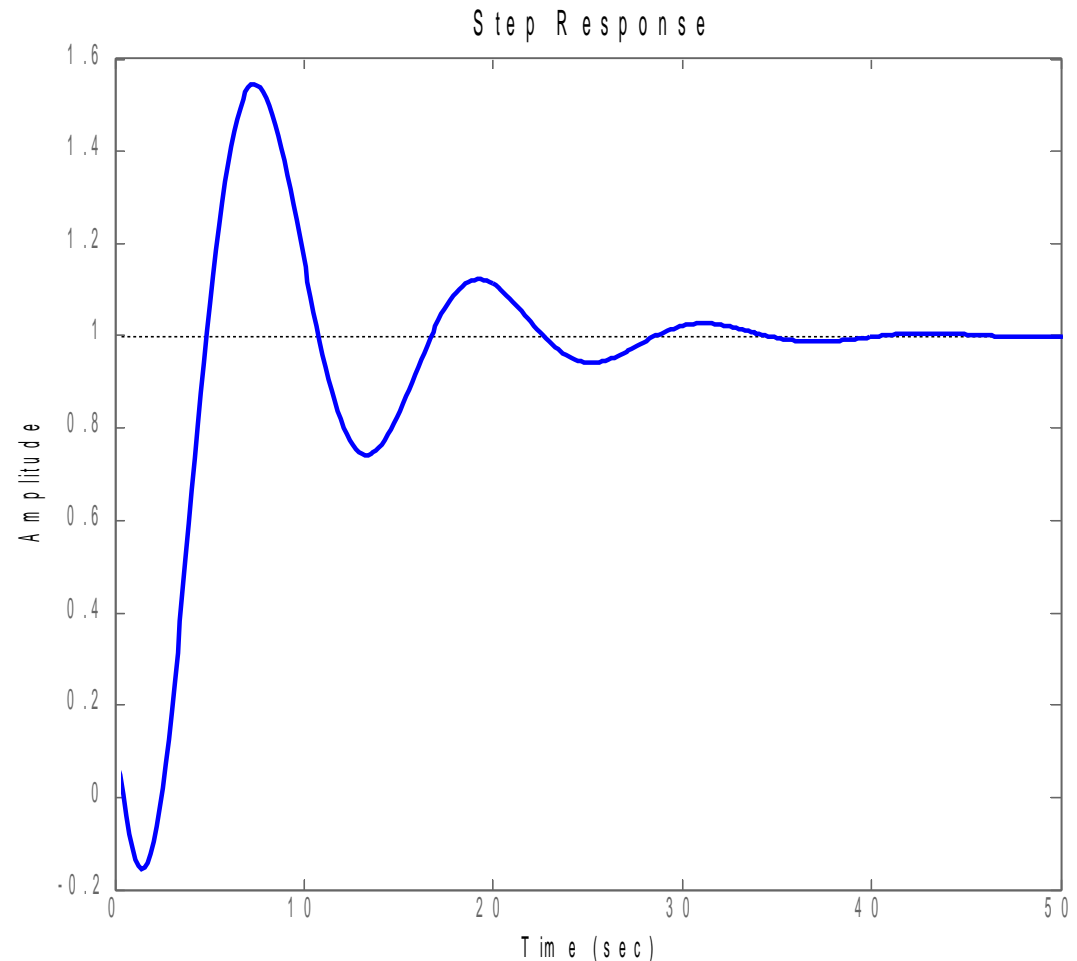
$$v_C = 1$$

$$P(s) = \frac{s-1}{(s+1)(s+5)}$$

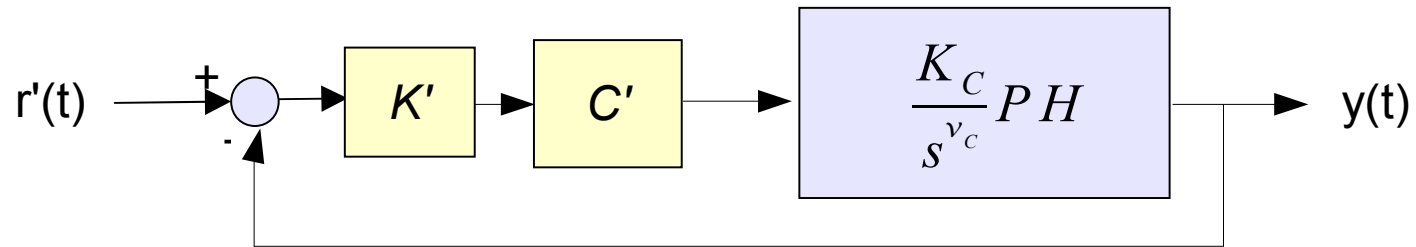
Inserire uno zero a parte reale positiva nel controllore

$$C(s) = K' \frac{s-2}{s}$$

$$K' = 1 \leq 1,53$$



## Criteri generali per la sintesi



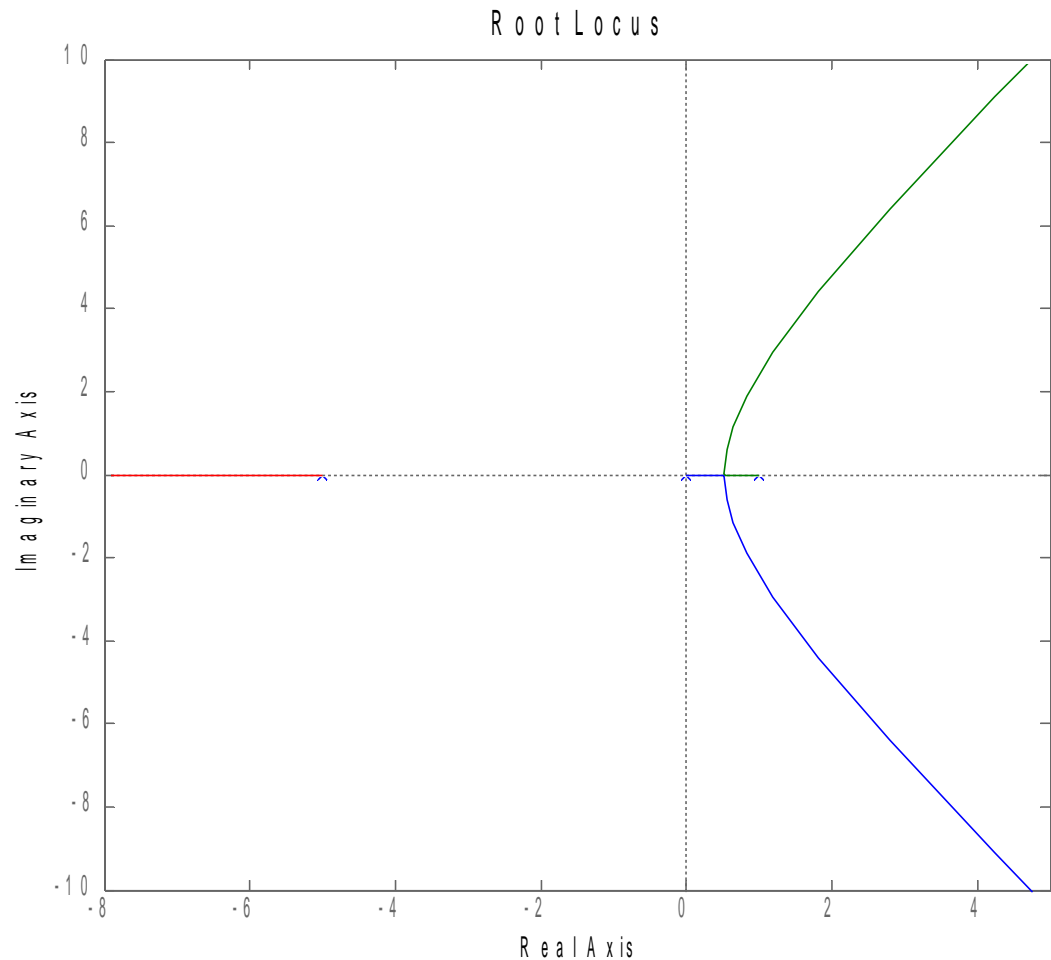
NON cancellare poli e zeri a parte reale positiva

$$H=1$$

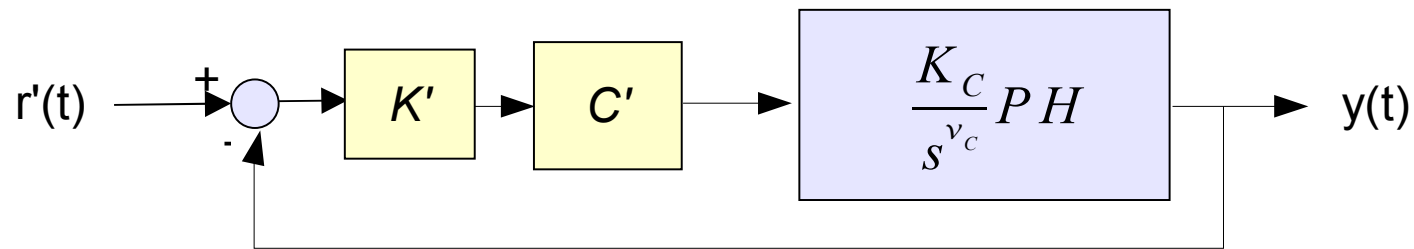
$$K_C=1$$

$$v_C=1$$

$$P(s)=\frac{1}{(s-1)(s+5)}$$



## Criteri generali per la sintesi



NON cancellare poli e zeri a parte reale positiva

$$H = 1$$

$$K_C = 1$$

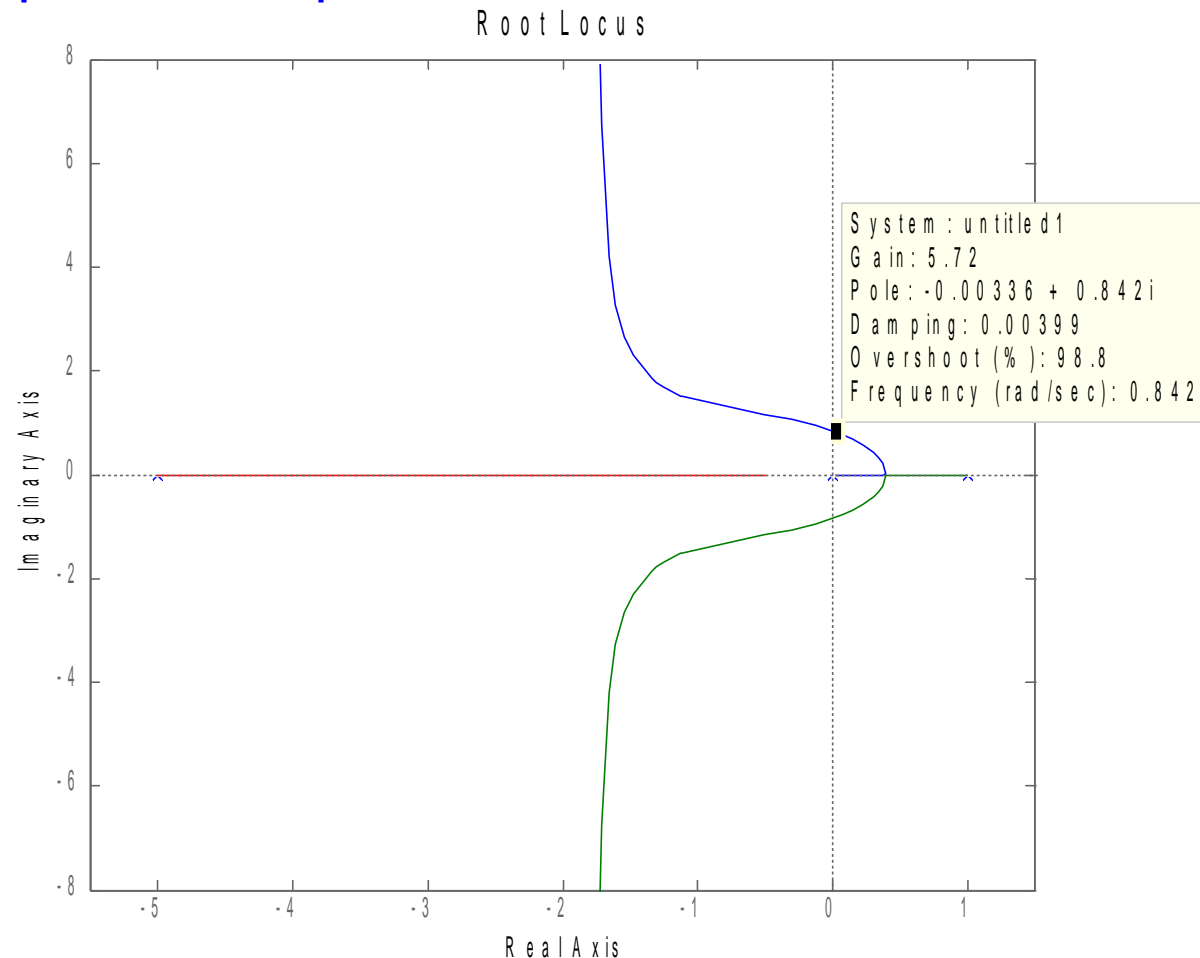
$$v_C = 1$$

$$P(s) = \frac{1}{(s-1)(s+5)}$$

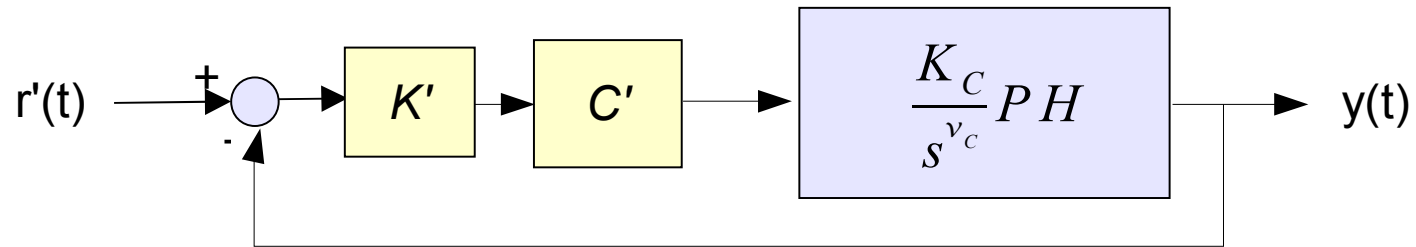
Inserire uno zero a parte reale negativa nel controllore

$$C(s) = K' \frac{s+0.5}{s}$$

$$K' \geq 5,72$$



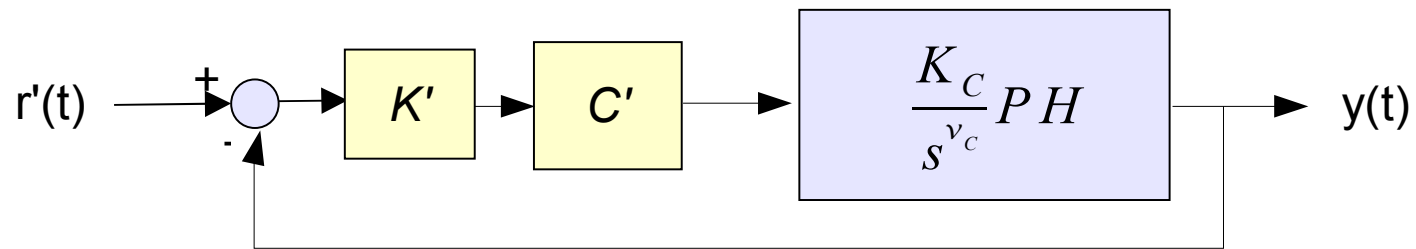
## Criteri generali per la sintesi



### NON cancellare poli a parte reale nulla

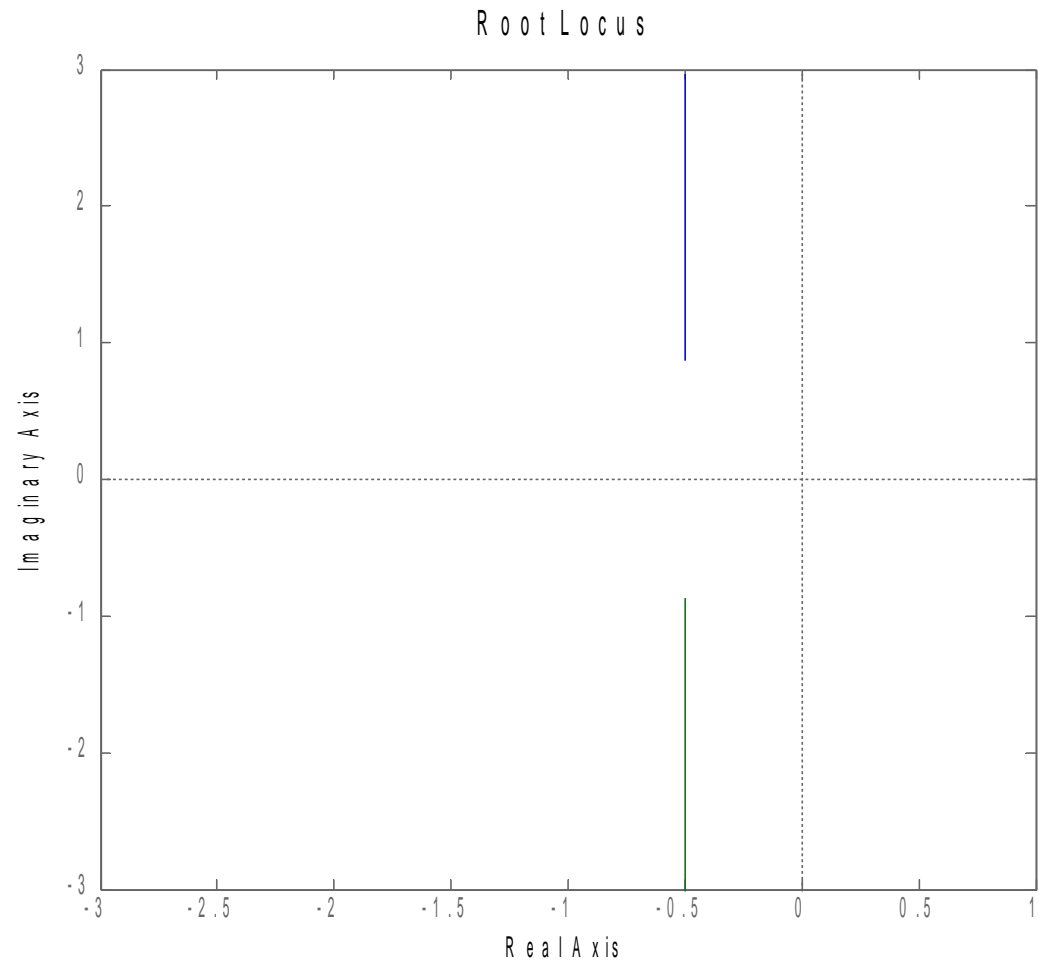
- La cancellazione di un polo nell'origine può causare il NON soddisfacimento delle specifiche sul comportamento a regime
- A causa di variazioni parametriche, il polo o lo zero a parte reale nulla introdotto o del sistema possono spostarsi nel semipiano positivo e originare un modo instabile
- L'introduzione del controllore deve anche garantire sufficienti margini di stabilità al sistema a ciclo chiuso: i suoi poli devono essere sufficientemente lontani dall'asse immaginario

## Criteri generali per la sintesi



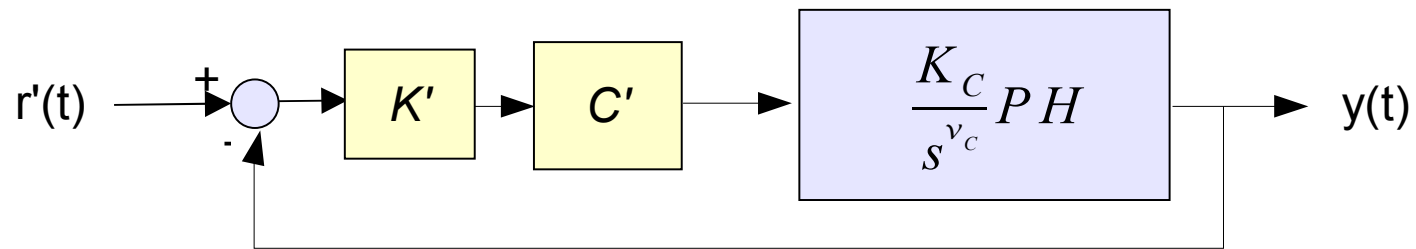
L'introduzione di un polo sposta il luogo delle radici verso il semipiano positivo

$$\begin{aligned} H &= 1 \\ K_C &= 1 \\ v_c &= 0 \\ P(s) &= \frac{1}{s^2 + s + 1} \end{aligned}$$



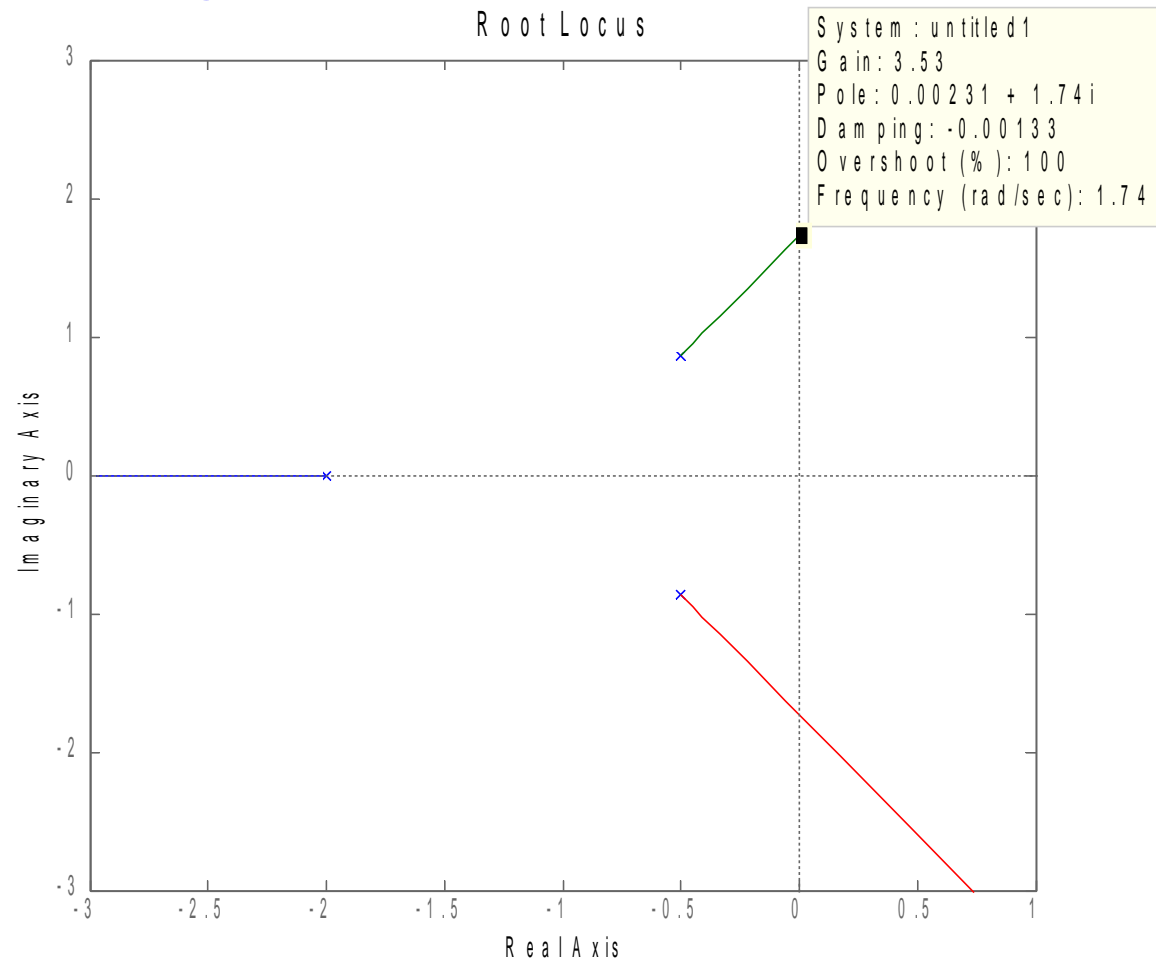


## Criteri generali per la sintesi

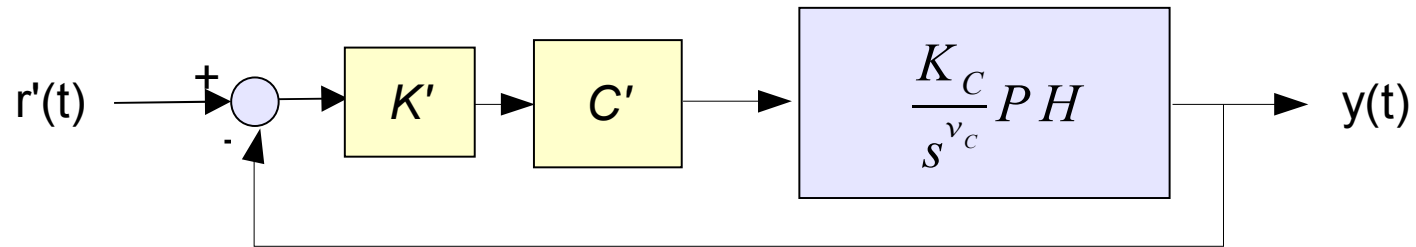


L'introduzione di un polo sposta il luogo delle radici verso il semipiano positivo

$$\begin{aligned}
 H &= 1 \\
 K_C &= 1 \\
 v_C &= 0 \\
 P(s) &= \frac{1}{s^2 + s + 1} \\
 C(s) &= K' \frac{1}{0.5s + 1} \\
 K' &= 1 \leq 3,53
 \end{aligned}$$



## Criteri generali per la sintesi



L'introduzione di un polo sposta il luogo delle radici verso il semipiano positivo

$$H = 1$$

$$K_C = 1$$

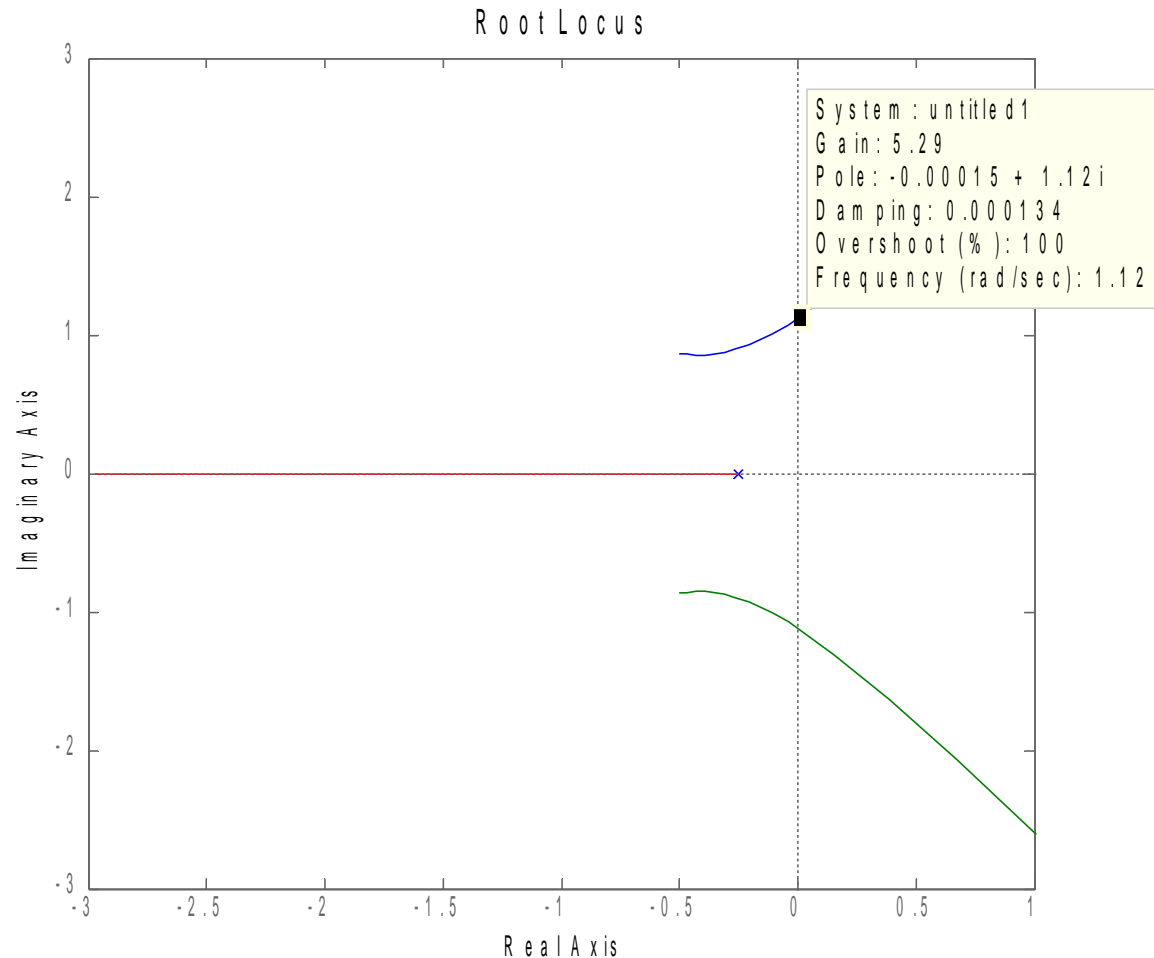
$$v_c = 0$$

$$P(s) = \frac{1}{s^2 + s + 1}$$

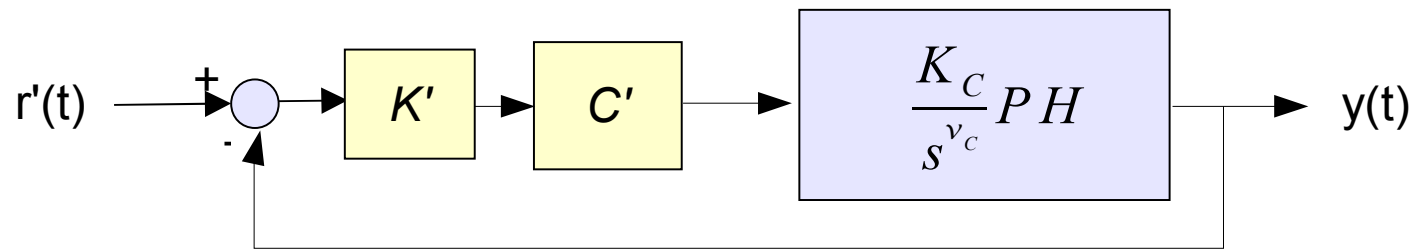
$$C(s) = K' \frac{1}{4s + 1}$$

$$K' = 1 \leq 3,29$$

Lo spostamento è tanto maggiore quanto il polo è vicino all'origine



## Criteri generali per la sintesi



L'introduzione di uno zero sposta il luogo delle radici verso il semipiano negativo

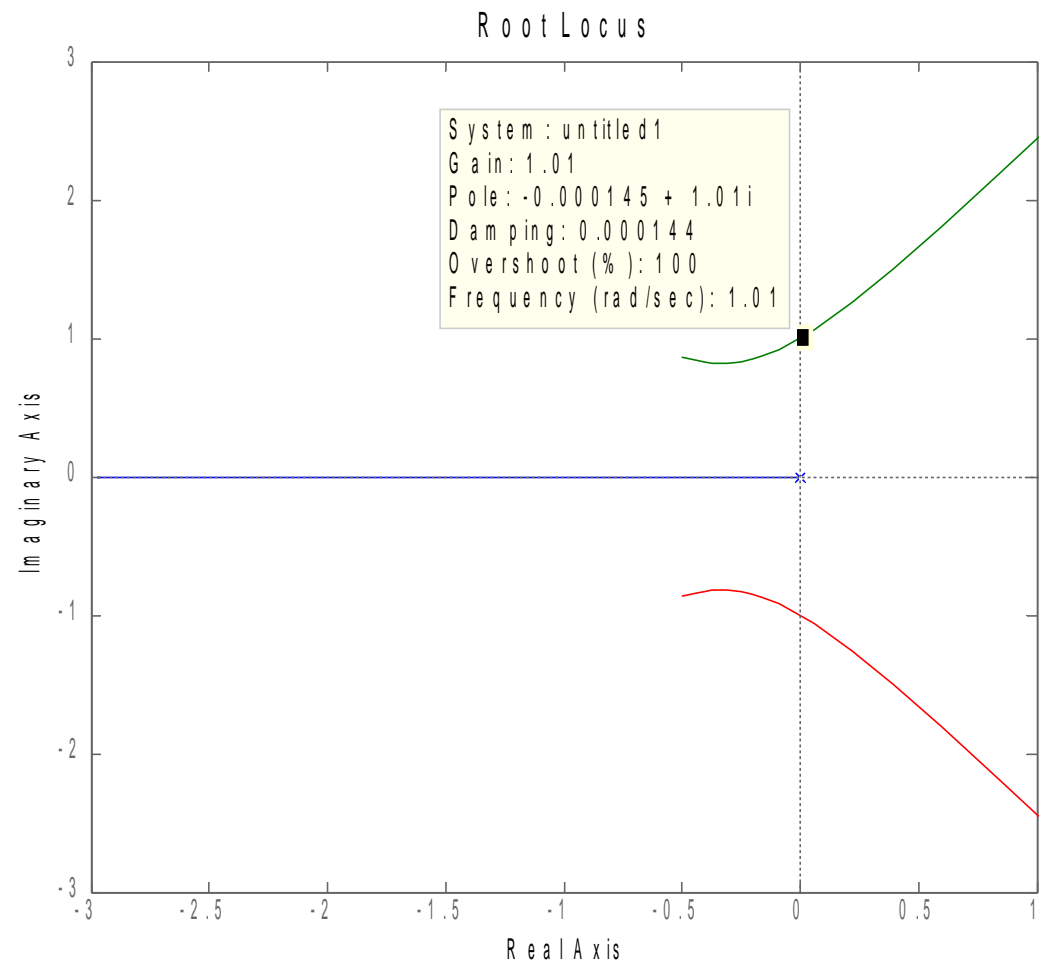
$$H=1$$

$$K_C=1$$

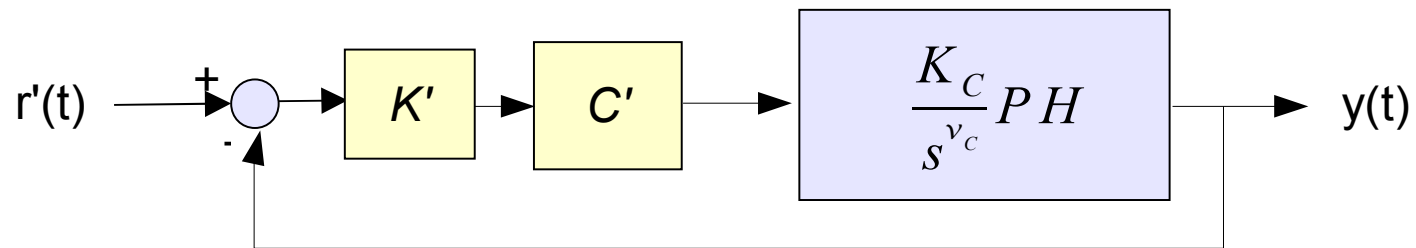
$$v_C=1$$

$$P(s)=\frac{1}{s^2+s+1}$$

$$K' \leq 1$$



## Criteri generali per la sintesi



L'introduzione di uno zero sposta il luogo delle radici verso il semipiano negativo

$$H = 1$$

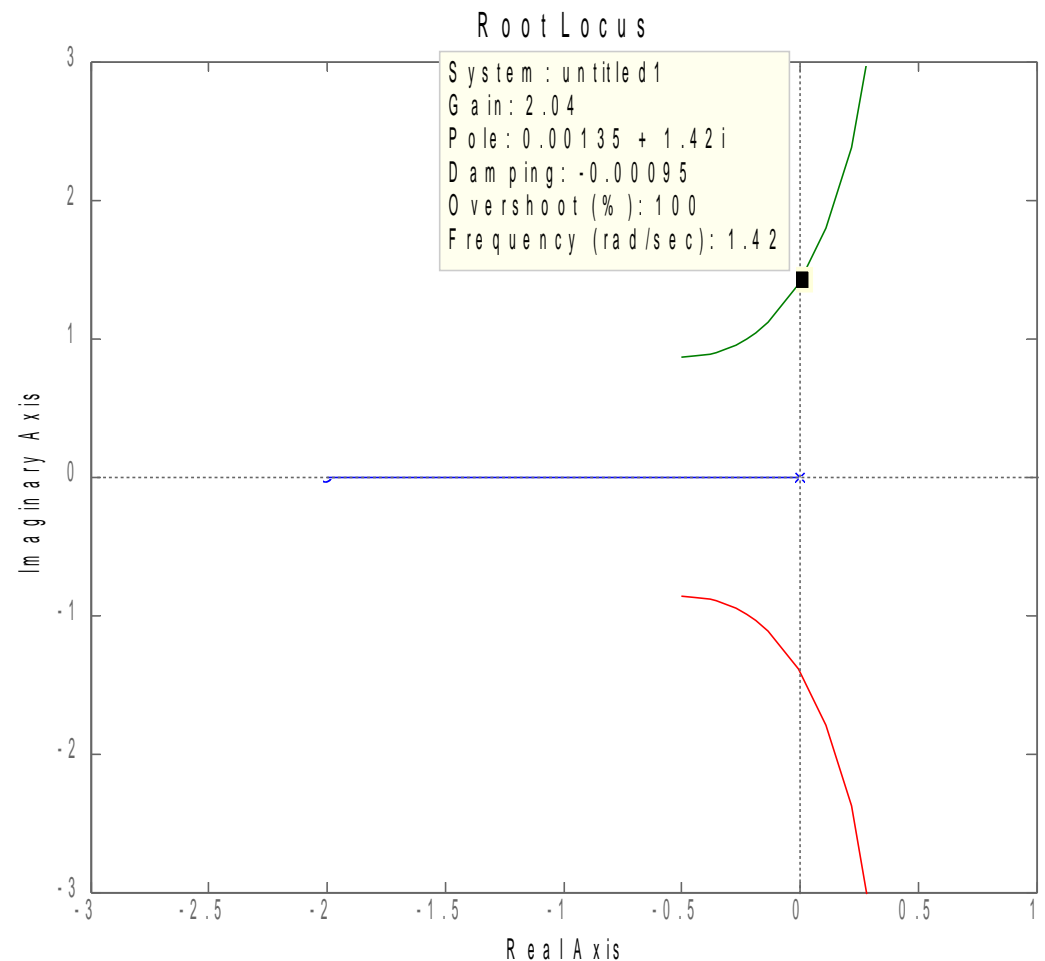
$$K_C = 1$$

$$v_C = 1$$

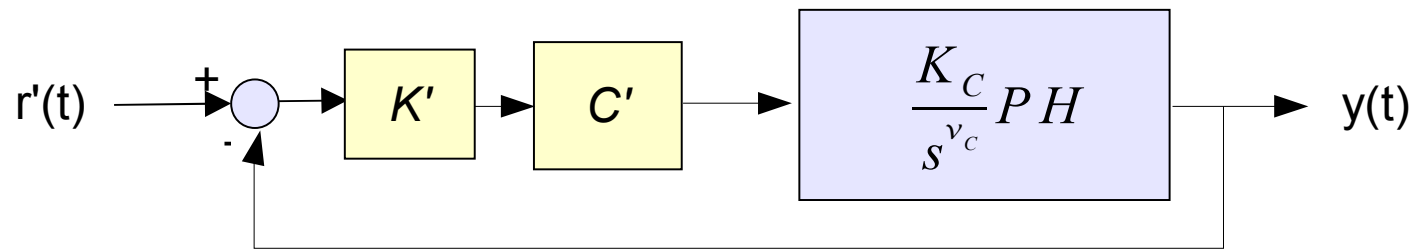
$$P(s) = \frac{1}{s^2 + s + 1}$$

$$C(s) = K' \frac{0.5s + 1}{s}$$

$$K' = 1 \leq 2$$



## Criteri generali per la sintesi



L'introduzione di uno zero sposta il luogo delle radici verso il semipiano negativo

$$H = 1$$

$$K_C = 1$$

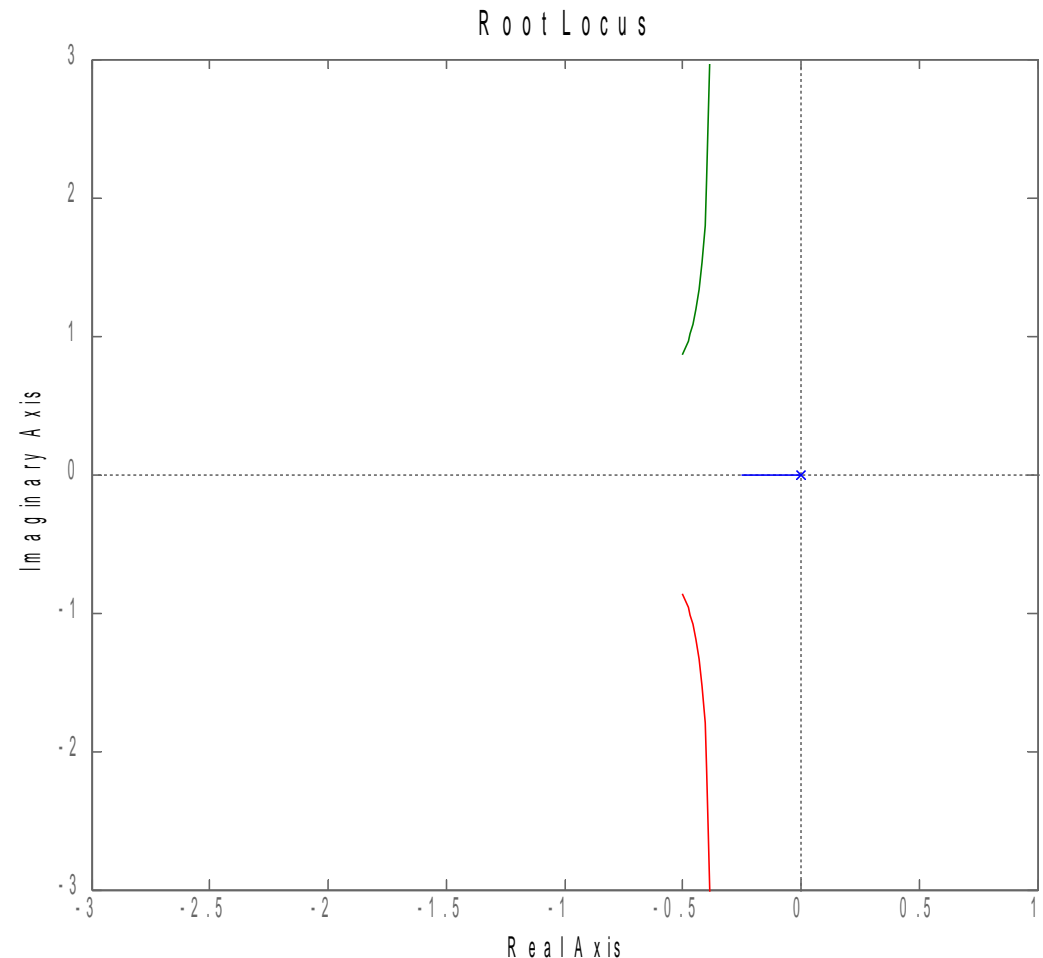
$$v_c = 1$$

$$P(s) = \frac{1}{s^2 + s + 1}$$

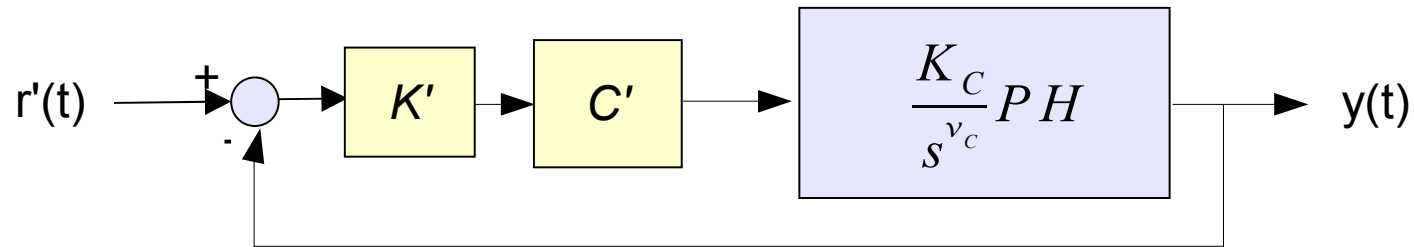
$$C(s) = K' \frac{4s + 1}{s}$$

$K'$  non limitato

Lo spostamento è tanto maggiore quanto lo zero è vicino all'origine



## Criteri generali per la sintesi



L'introduzione di una coppia polo - zero vicino all'origine tende a modificare la taratura del luogo in modo da avere un guadagno critico inferiore

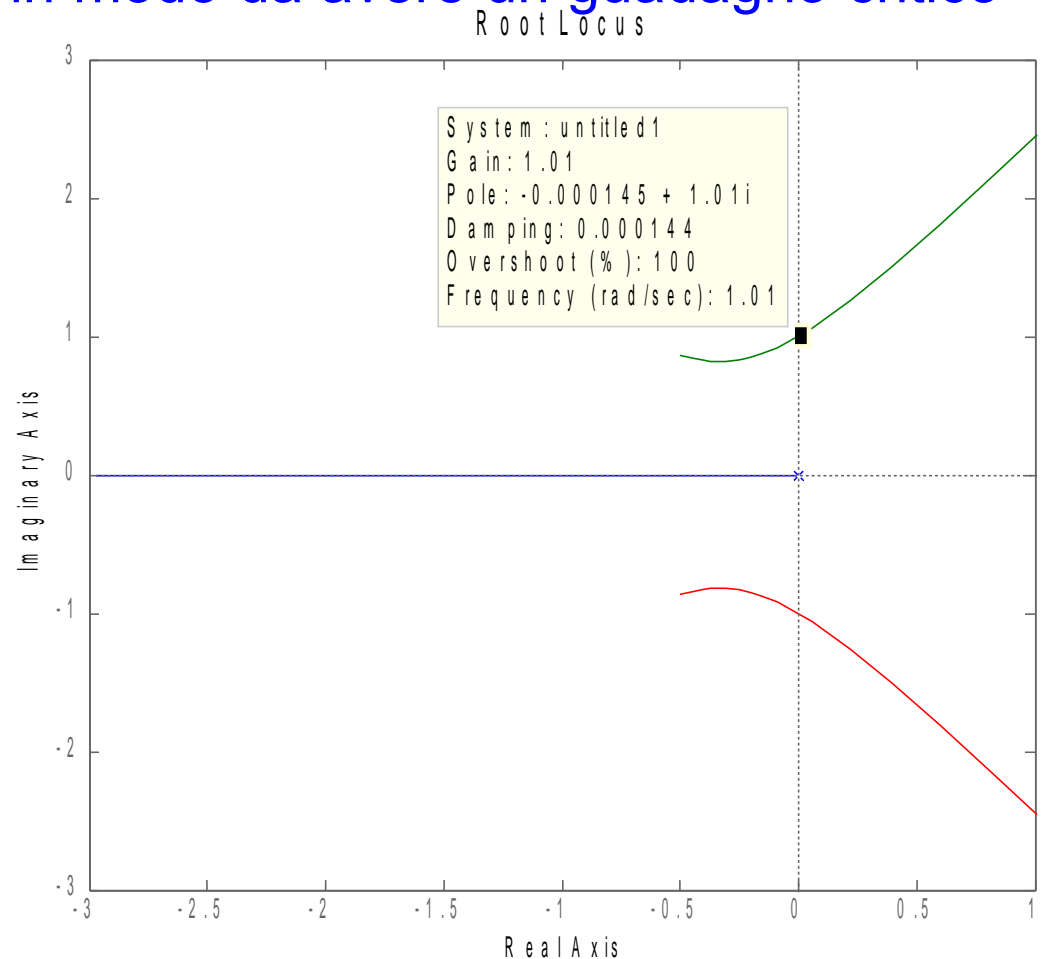
$$H = 1$$

$$K_C = 1$$

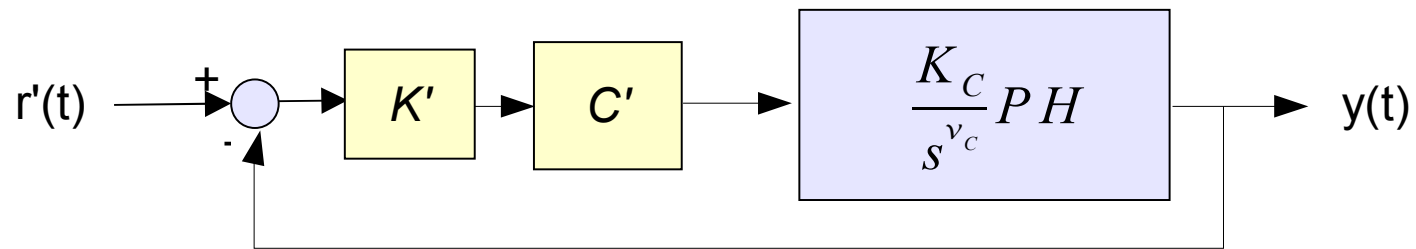
$$v_C = 1$$

$$P(s) = \frac{1}{s^2 + s + 1}$$

$$K' \leq 1$$



## Criteri generali per la sintesi



L'introduzione di una coppia polo - zero vicino all'origine tende a modificare la taratura del luogo in modo da avere un guadagno critico inferiore

$$H = 1$$

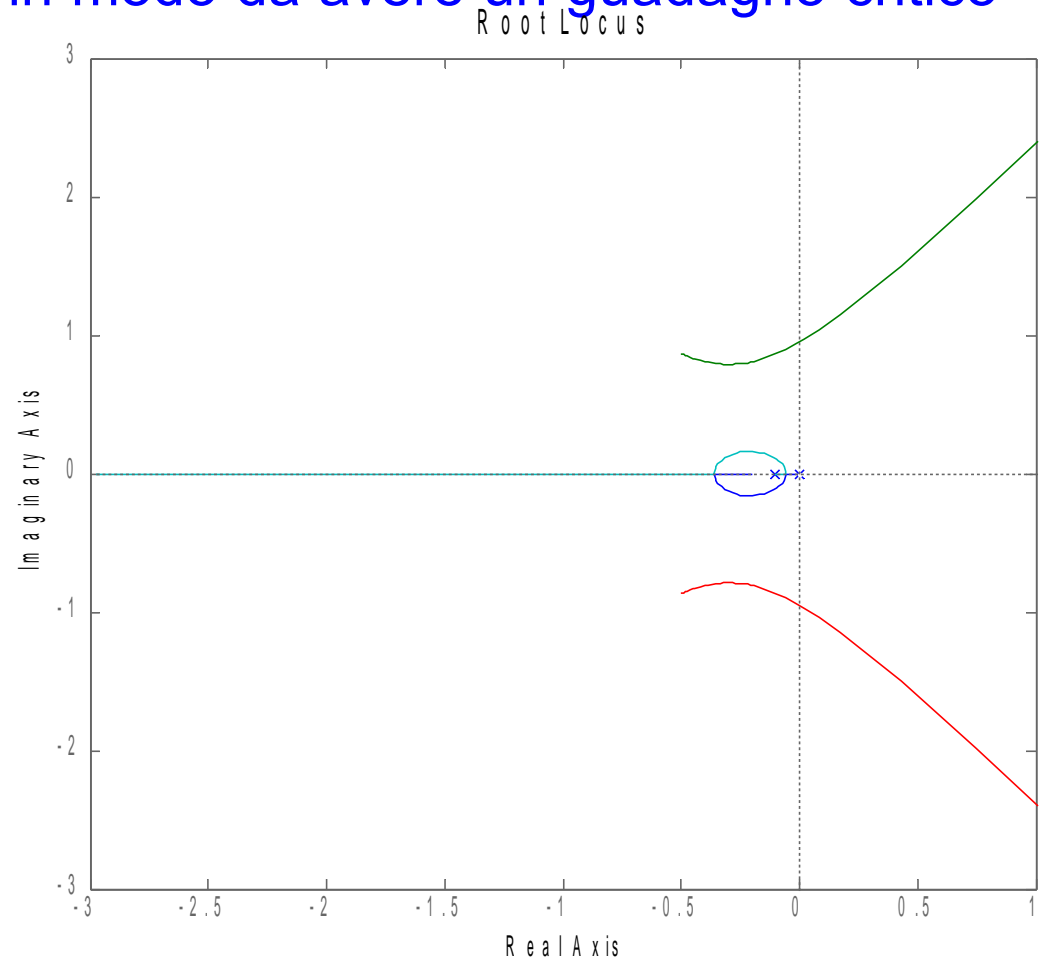
$$K_C = 1$$

$$v_c = 1$$

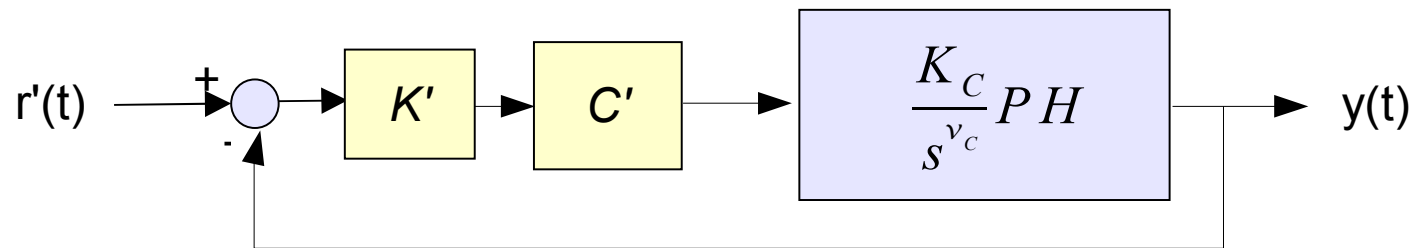
$$P(s) = \frac{1}{s^2 + s + 1}$$

$$K' \leq 1,79$$

$$C(s) = K' \frac{5s + 1}{s(10s + 1)}$$



## Criteri generali per la sintesi



L'introduzione di una coppia polo - zero vicino all'origine tende a modificare la taratura del luogo in modo da avere un guadagno critico inferiore

$$H=1$$

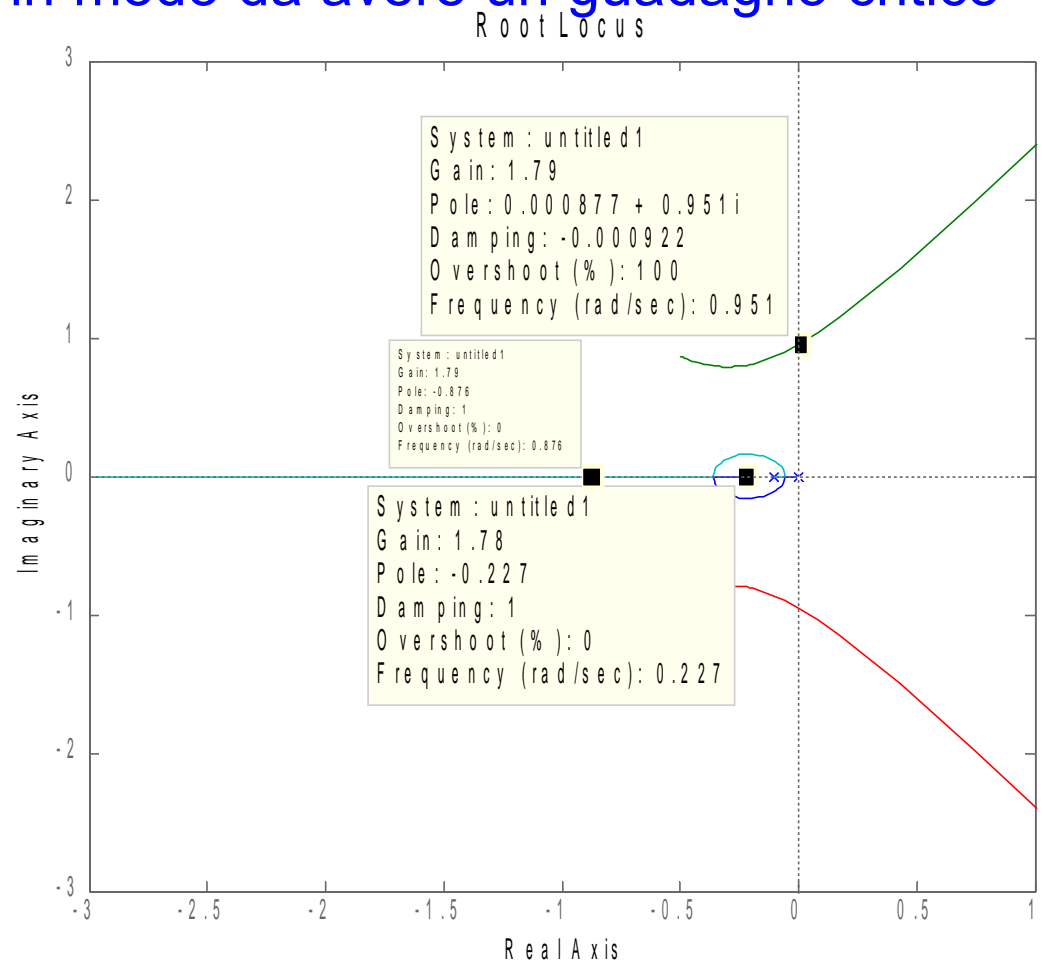
$$K_C=1$$

$$v_c=1$$

$$P(s)=\frac{1}{s^2+s+1}$$

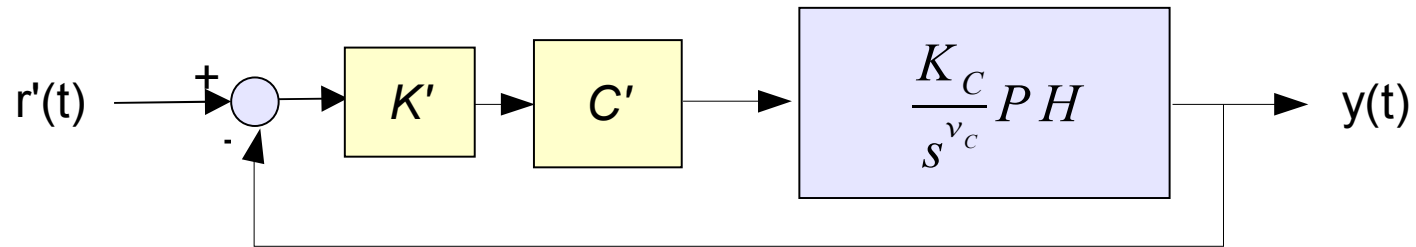
$$K' \leq 1,79$$

$$C(s)=K' \frac{5s+1}{s(10s+1)}$$





## Criteri generali per la sintesi



L'introduzione di una coppia zero - polo vicino all'origine modifica la taratura del luogo in modo da avere uno spostamento verso sinistra a parità di guadagno critico

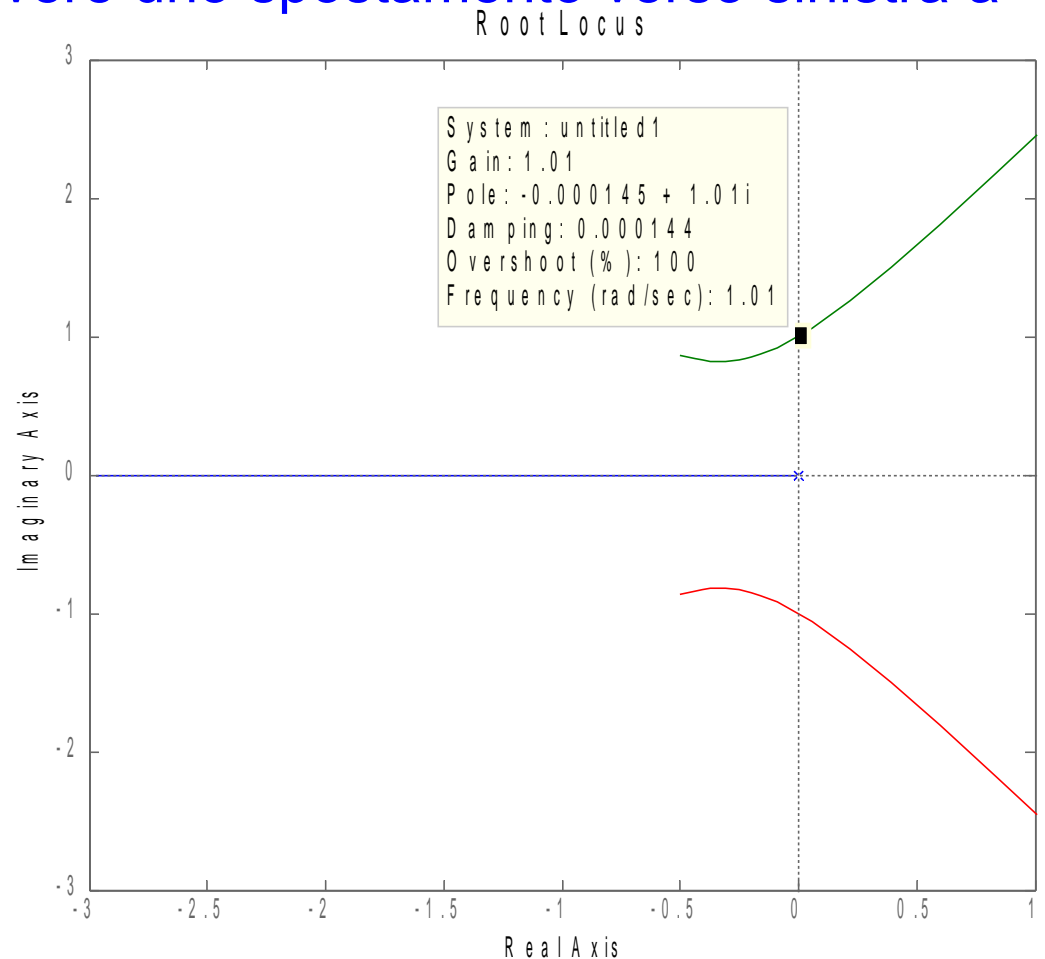
$$H=1$$

$$K_C=1$$

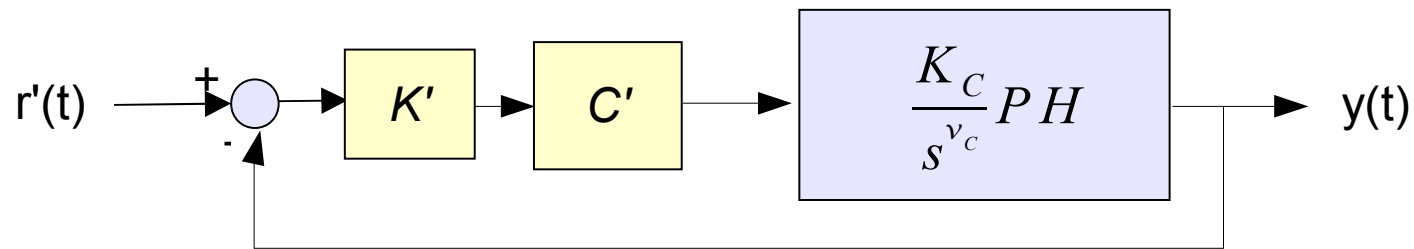
$$v_C=1$$

$$P(s)=\frac{1}{s^2+s+1}$$

$$K' \leq 1$$



## Criteri generali per la sintesi



L'introduzione di una coppia zero - polo vicino all'origine modifica la taratura del luogo in modo da avere uno spostamento verso sinistra a parità di guadagno critico

$$H=1$$

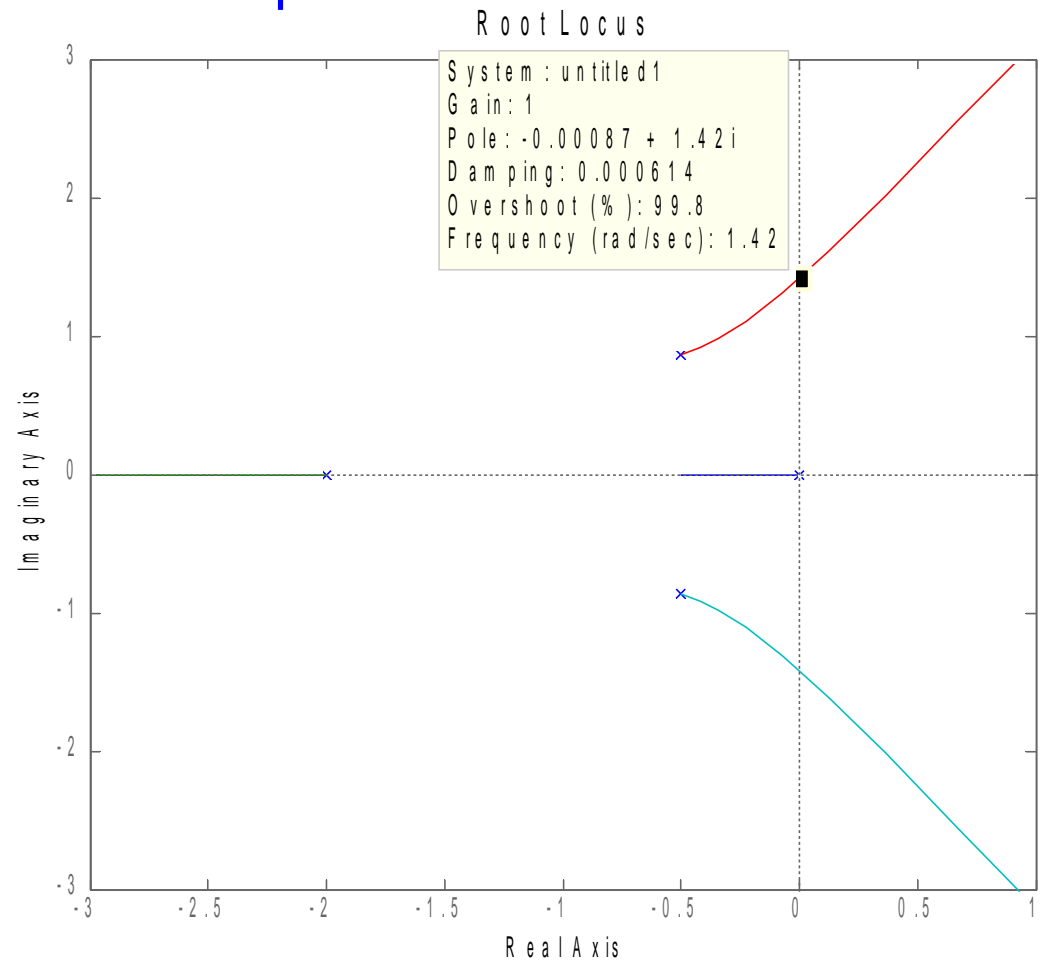
$$K_C=1$$

$$v_C=1$$

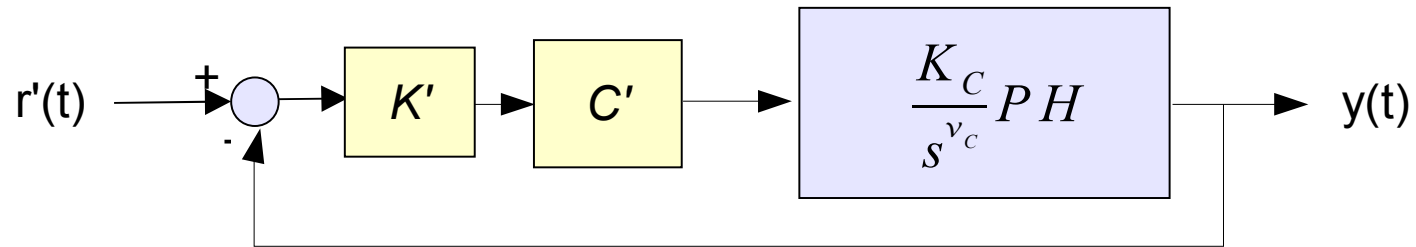
$$P(s)=\frac{1}{s^2+s+1}$$

$$K' \leq 1$$

$$C(s)=K' \frac{5s+1}{s(0,5s+1)}$$



## Criteri generali per la sintesi



La cancellazione di parte del processo può consentire la modifica del luogo delle radici per rispettare le specifiche

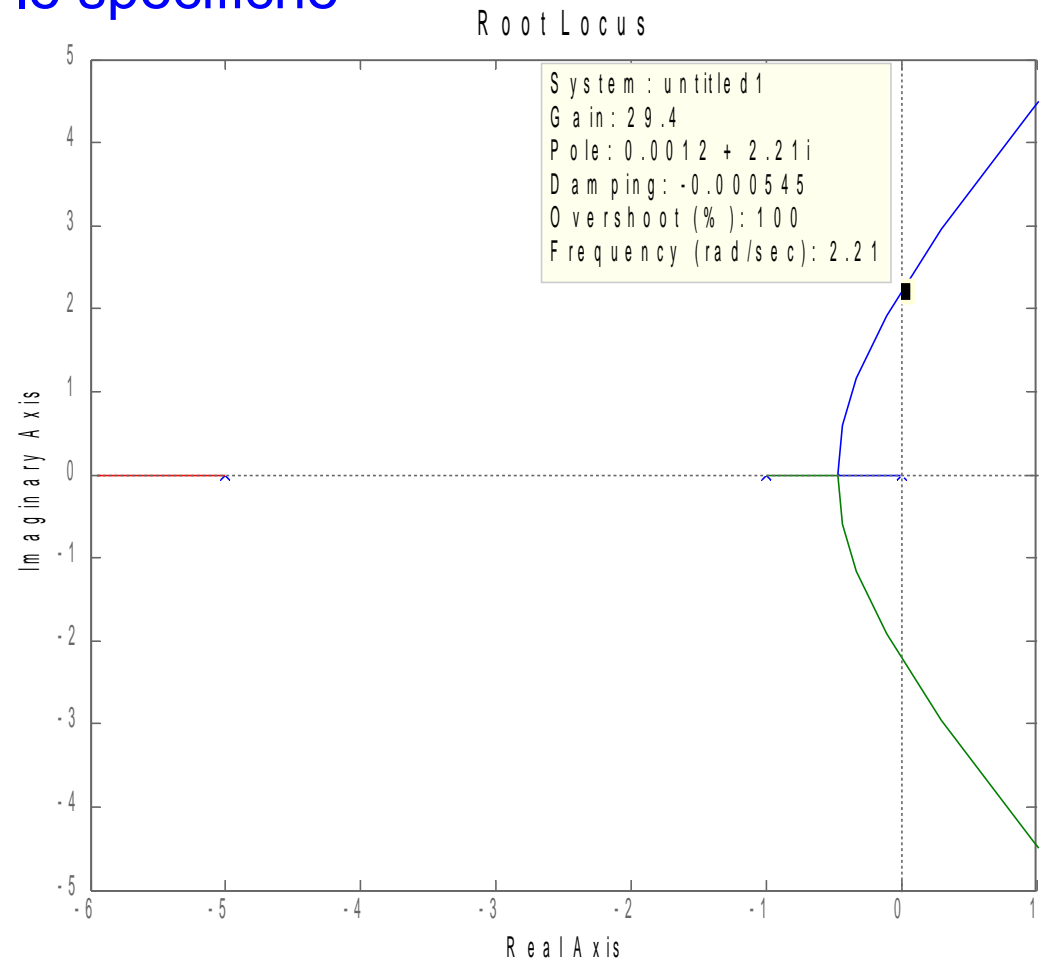
$$H=1$$

$$K_C=1$$

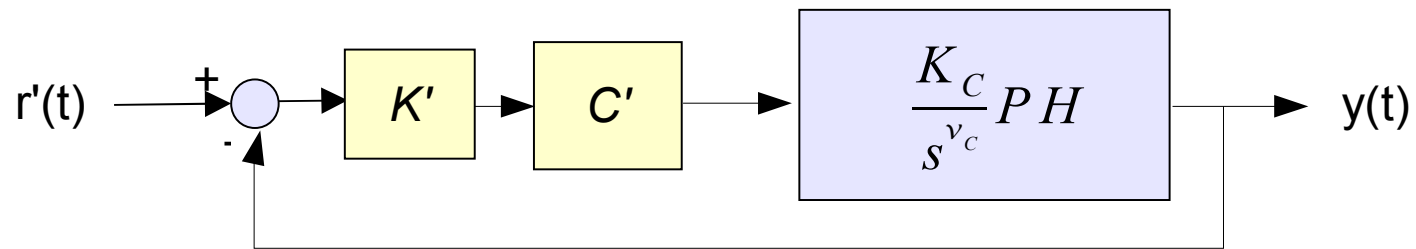
$$v_C=1$$

$$P(s)=\frac{1}{(s+1)(s+5)}$$

$$K' \leq 29,4$$



## Criteri generali per la sintesi



La cancellazione di parte del processo può consentire la modifica del luogo delle radici per rispettare le specifiche

$$H=1$$

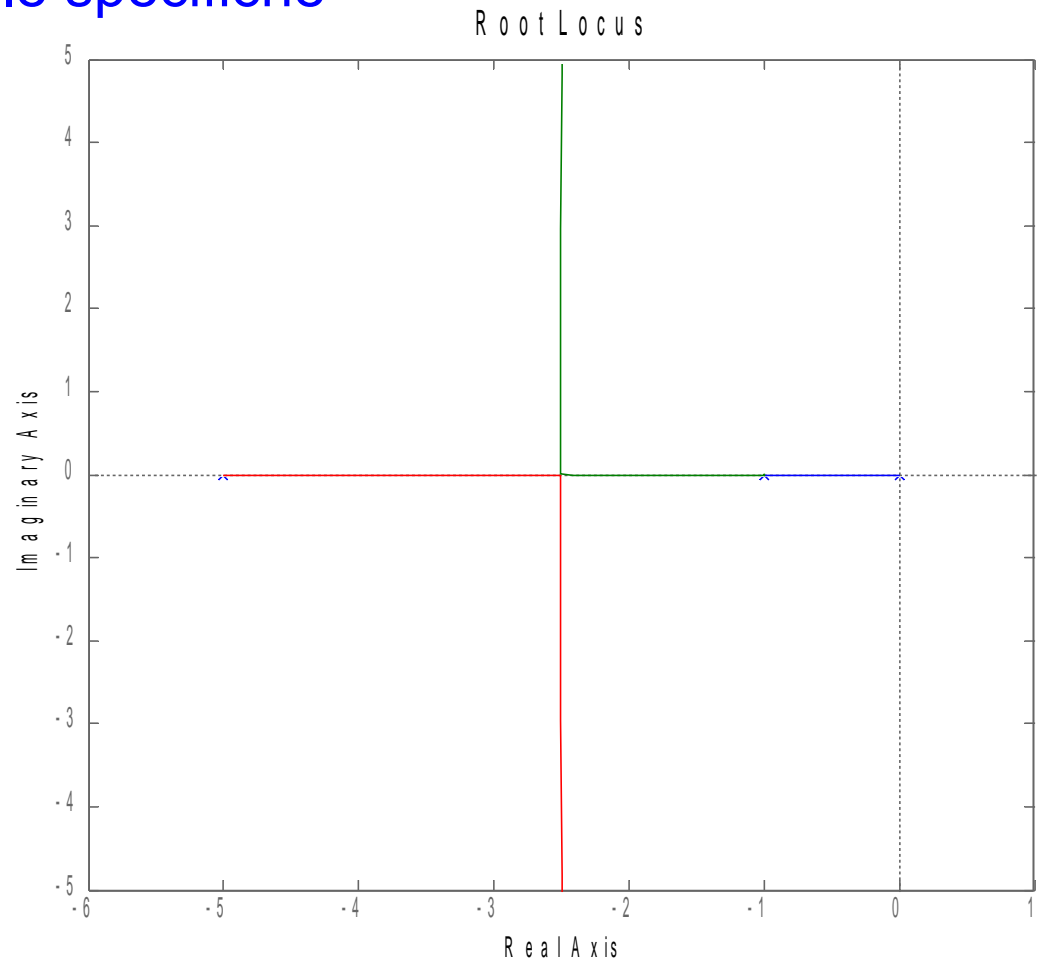
$$K_C=1$$

$$v_C=1$$

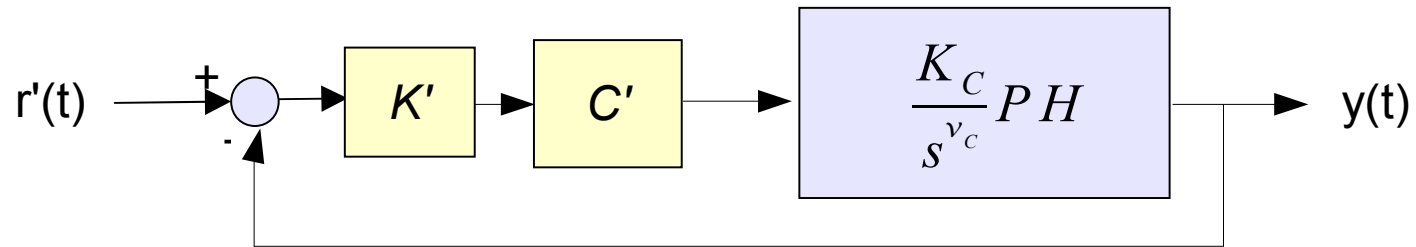
$$P(s)=\frac{1}{(s+1)(s+5)}$$

$K'$  non limitato

$$C(s)=K' \frac{s+1}{s}$$



## Esempio



$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}$$

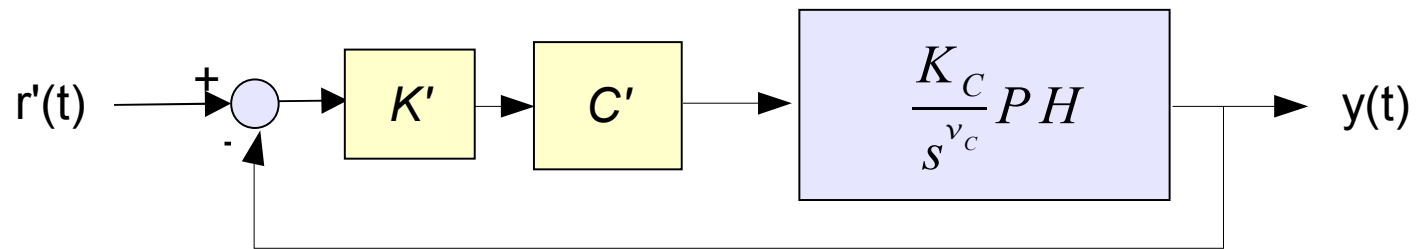
$$K_{W_r} = 0,5$$

$$|e_{\infty}(t)| = |e_{r_{\infty}}(t)|_{\delta_{-2}} + |e_{d_{\infty}}(t)|_{\delta_{-1}} \leq 0,1$$

$$t_{a_{1^{\circ}/_o}} \leq 2$$

$$s_{o/_o} \leq 5^{\circ}/_o$$

## Esempio



$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}$$

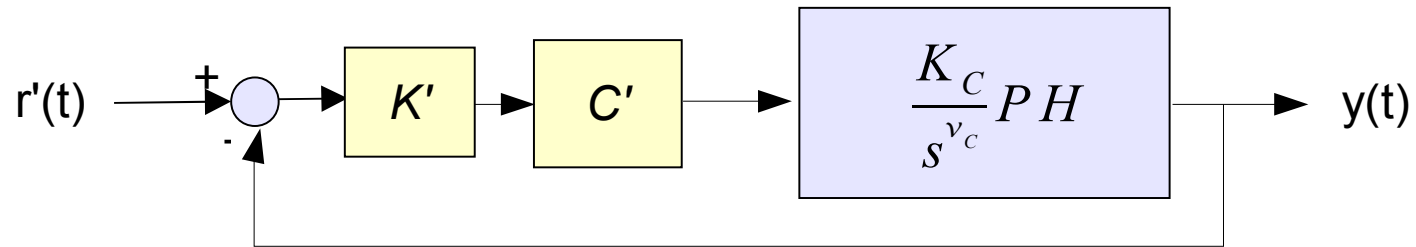
$$K_{W_r} = 0,5 \Rightarrow K_d = 0,5 \Rightarrow H = 2$$

$$|e_{\infty}(t)| = |e_{r_{\infty}}(t)|_{\delta_{-2}} + |e_{d_{\infty}}(t)|_{\delta_{-1}} \leq 0,1 \Rightarrow \begin{matrix} v_c = 1 \\ K_C \geq 5 \end{matrix}$$

$$t_{a_{1\%}} \leq 2 \Rightarrow \tau_{eq} \leq \frac{2}{5} \Rightarrow \bar{\alpha} = 2,5$$

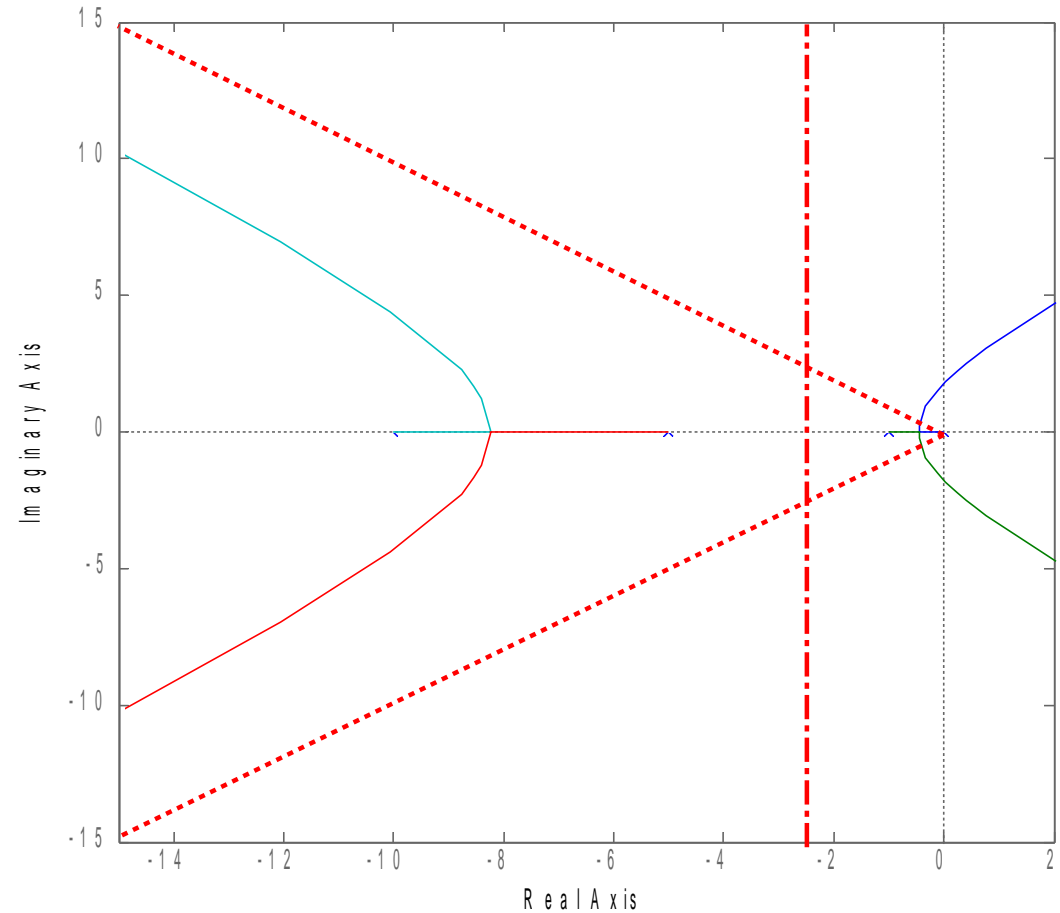
$$s_{ol_o} \leq 5^\circ / _o \Rightarrow \xi \geq 0,7 \Rightarrow \bar{\psi} = \frac{\pi}{4}$$

## Esempio



$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}; \quad H=2; \quad K_C=5; \quad v_C=1$$

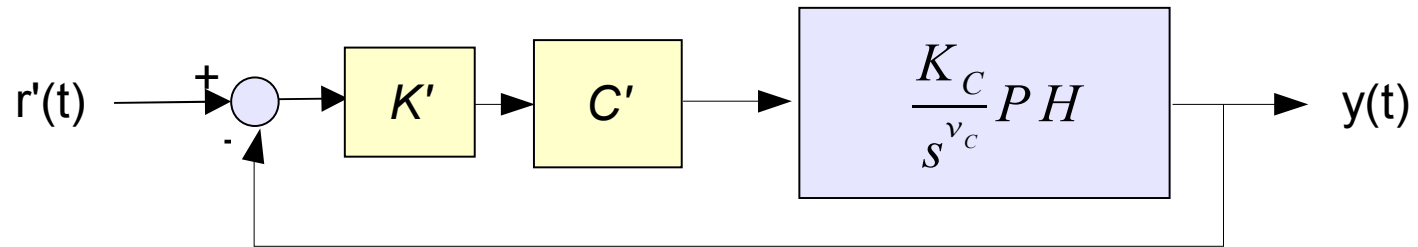
Root Locus



$$t_{a_{1\%}} \leq 2 \Rightarrow \tau_{eq} \leq \frac{2}{5} \Rightarrow \bar{\alpha} = 2,5$$

$$s_{ol_o} \leq 5^\circ / _o \Rightarrow \xi \geq 0,7 \Rightarrow \bar{\psi} = \frac{\pi}{4}$$

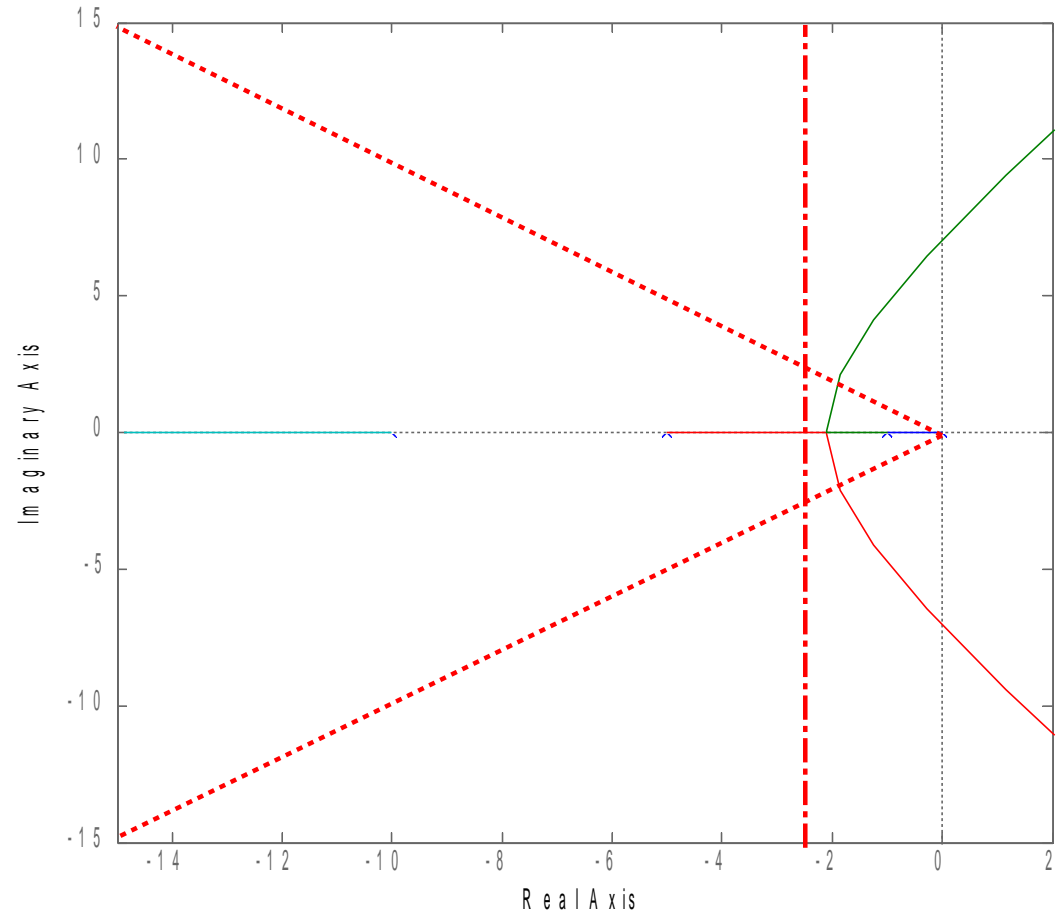
## Esempio



$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}; \quad H=2; \quad K_C=5; \quad v_C=1$$

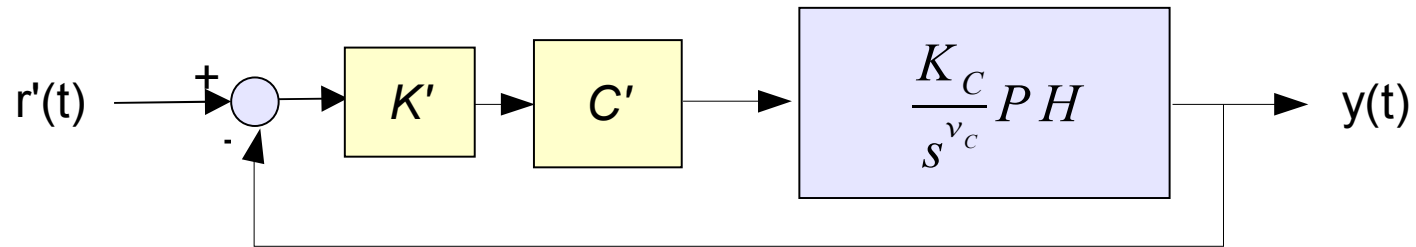
Root Locus

$$C(s) = 5 \frac{s+1}{s}$$



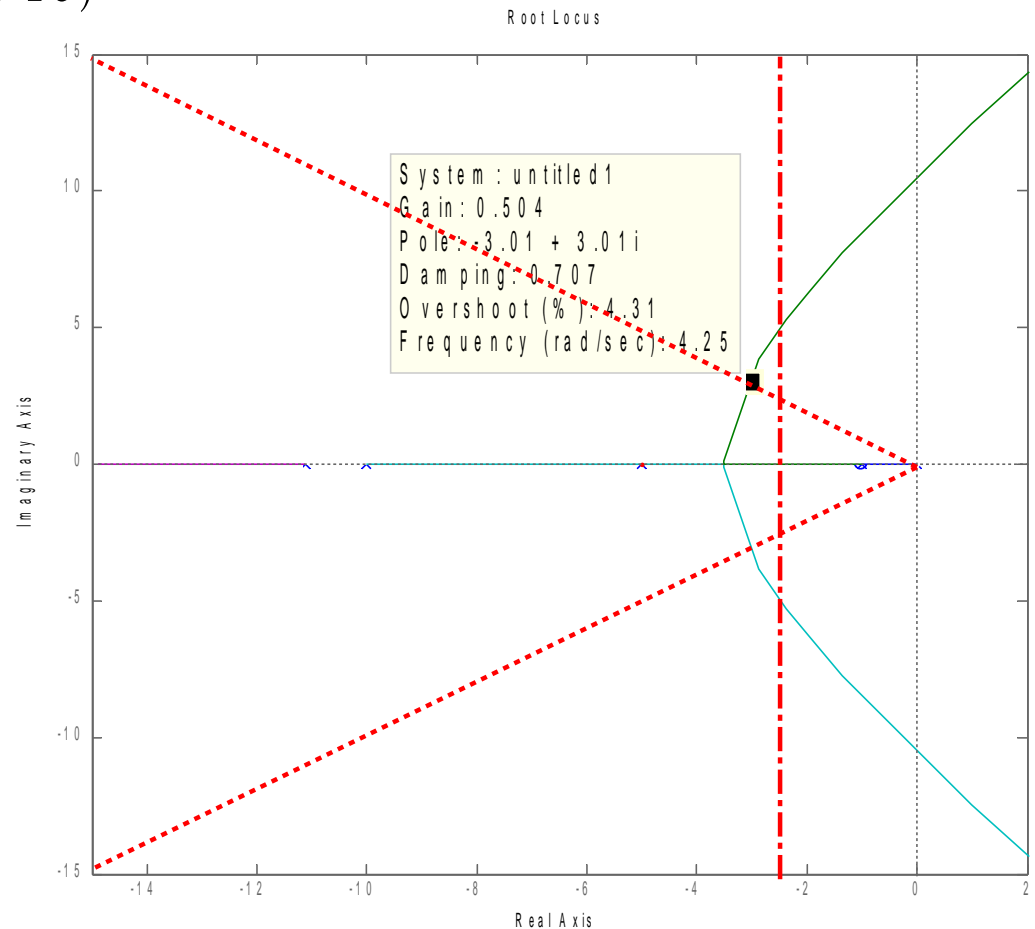


## Esempio

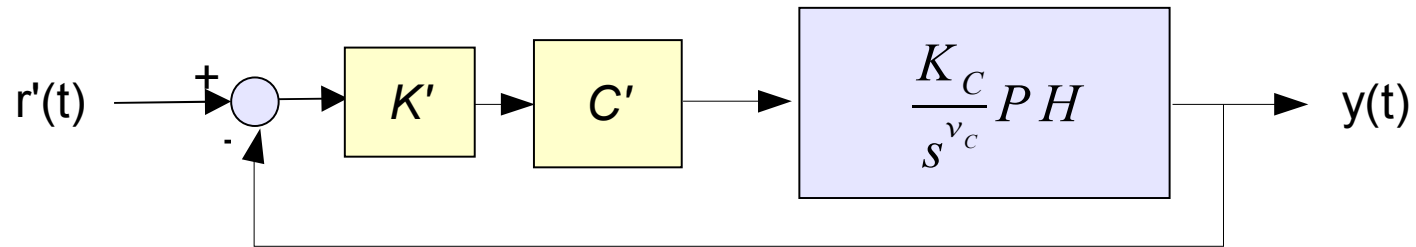


$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}; \quad H=2; \quad K_C=5; \quad v_C=1$$

$$C(s) = 5 \frac{(s+1)(0.2s+1)}{s(0.09s+1)}$$

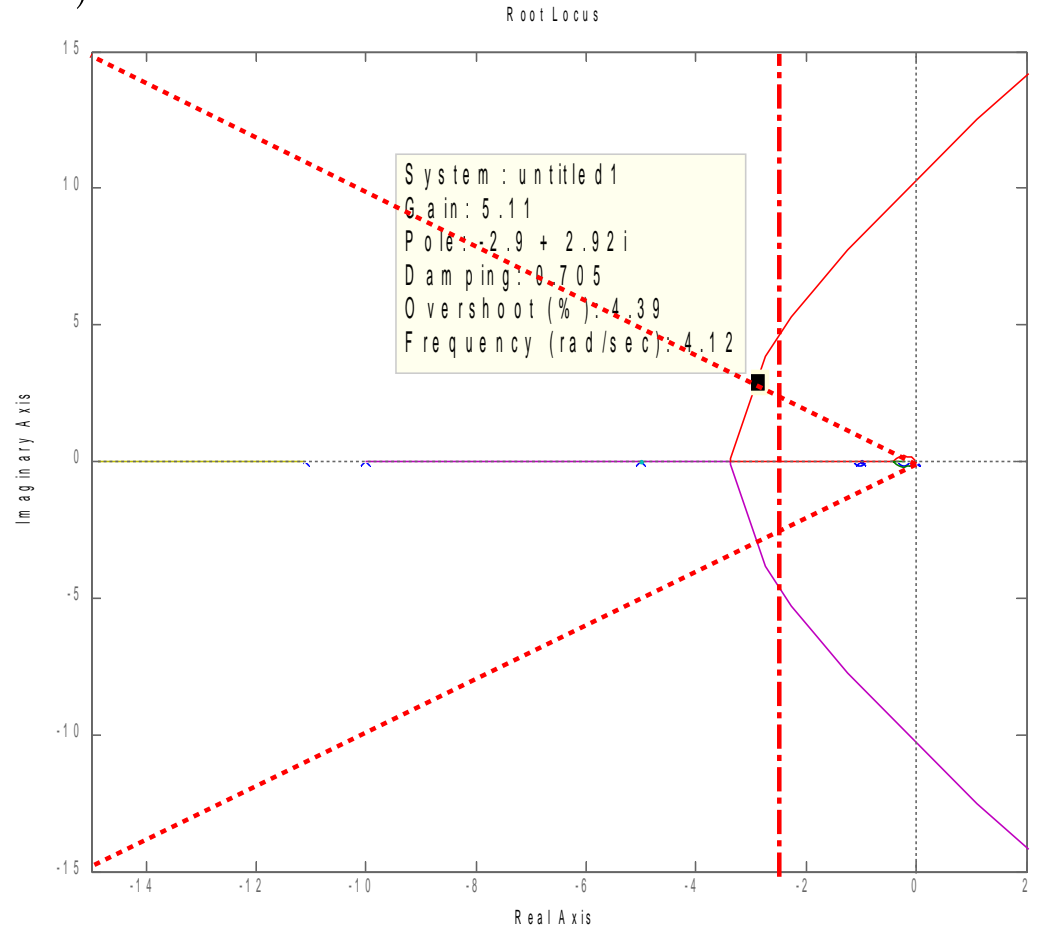


## Esempio

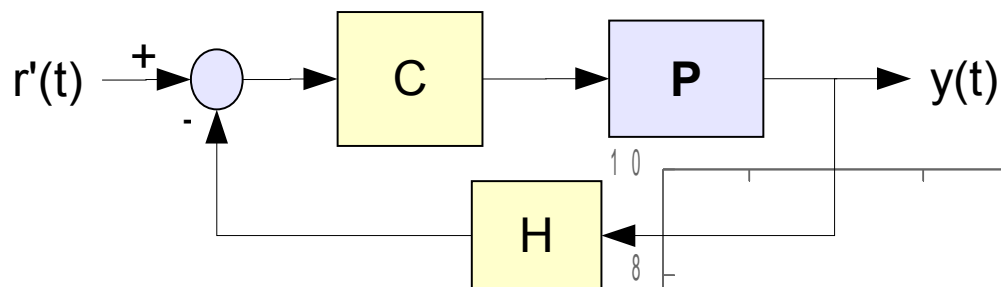


$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}; \quad H=2; \quad K_C=5; \quad v_c=1$$

$$C(s) = 5 \frac{(5s+1)(s+1)(0.2s+1)}{s(50s+1)(0.09s+1)}$$



# Esempio



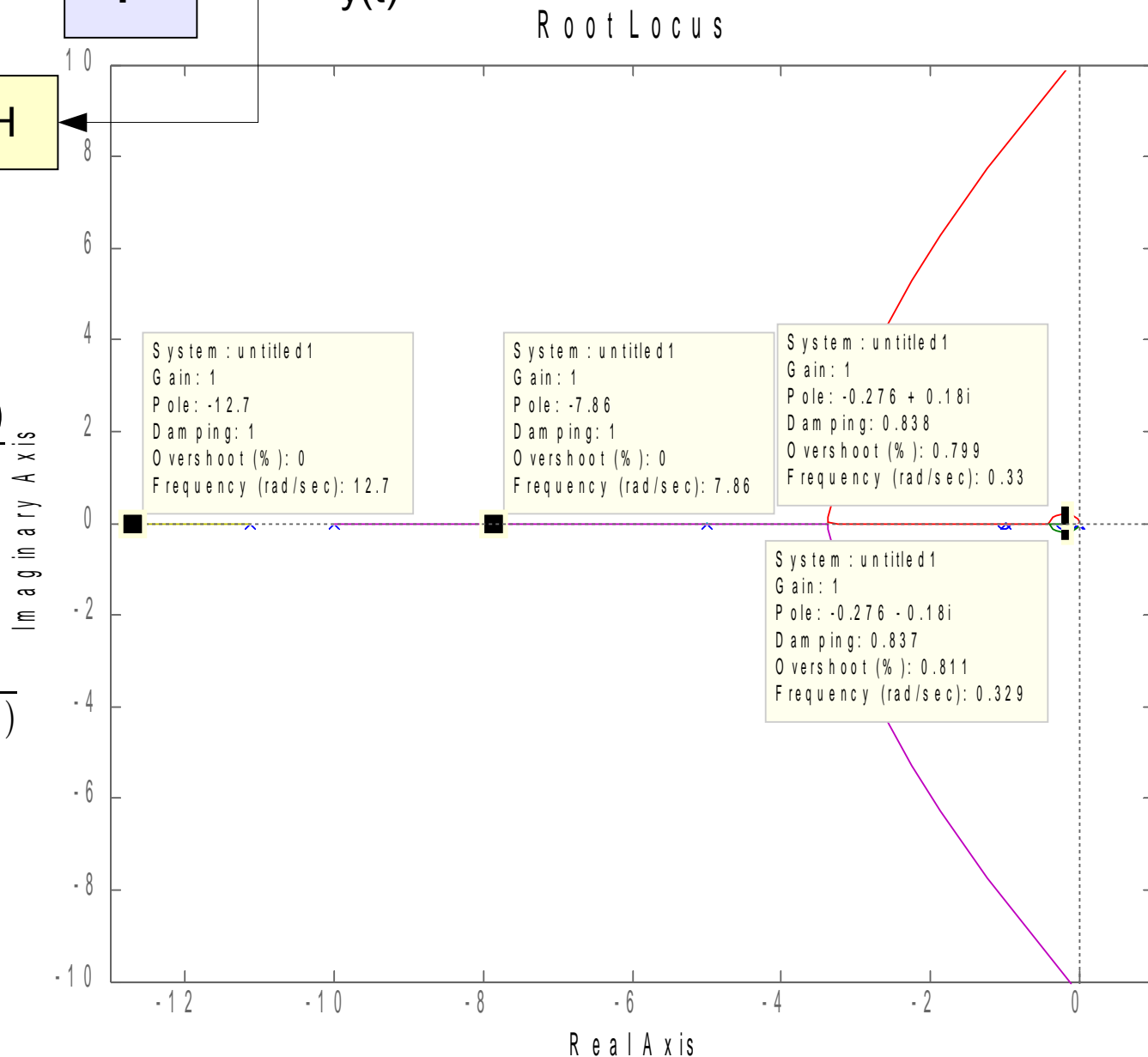
$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}$$

$$H = 2$$

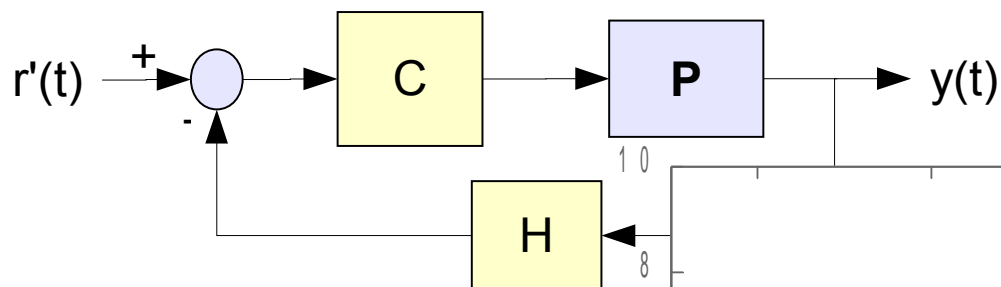
$$C(s) = 5 \frac{(5s+1)(s+1)(0.2s+1)}{s(50s+1)(0.09s+1)}$$

$$F(s) = \frac{50(5s+1)}{s(50s+1)(0.09s+1)(s+10)}$$

Il guadagno non è sufficiente ed il modo dominante è troppo in bassa frequenza



# Esempio



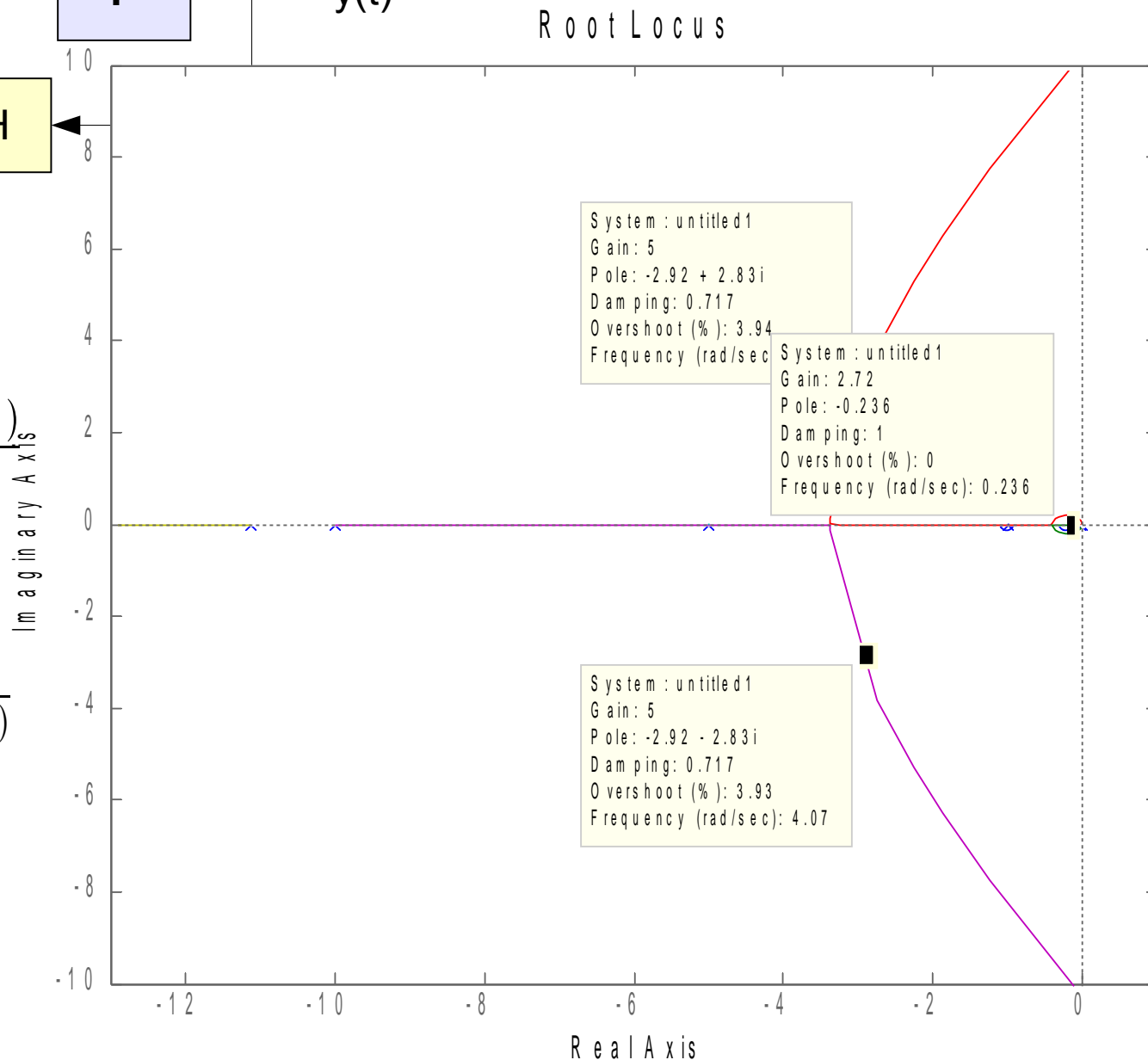
$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}$$

$$H = 2$$

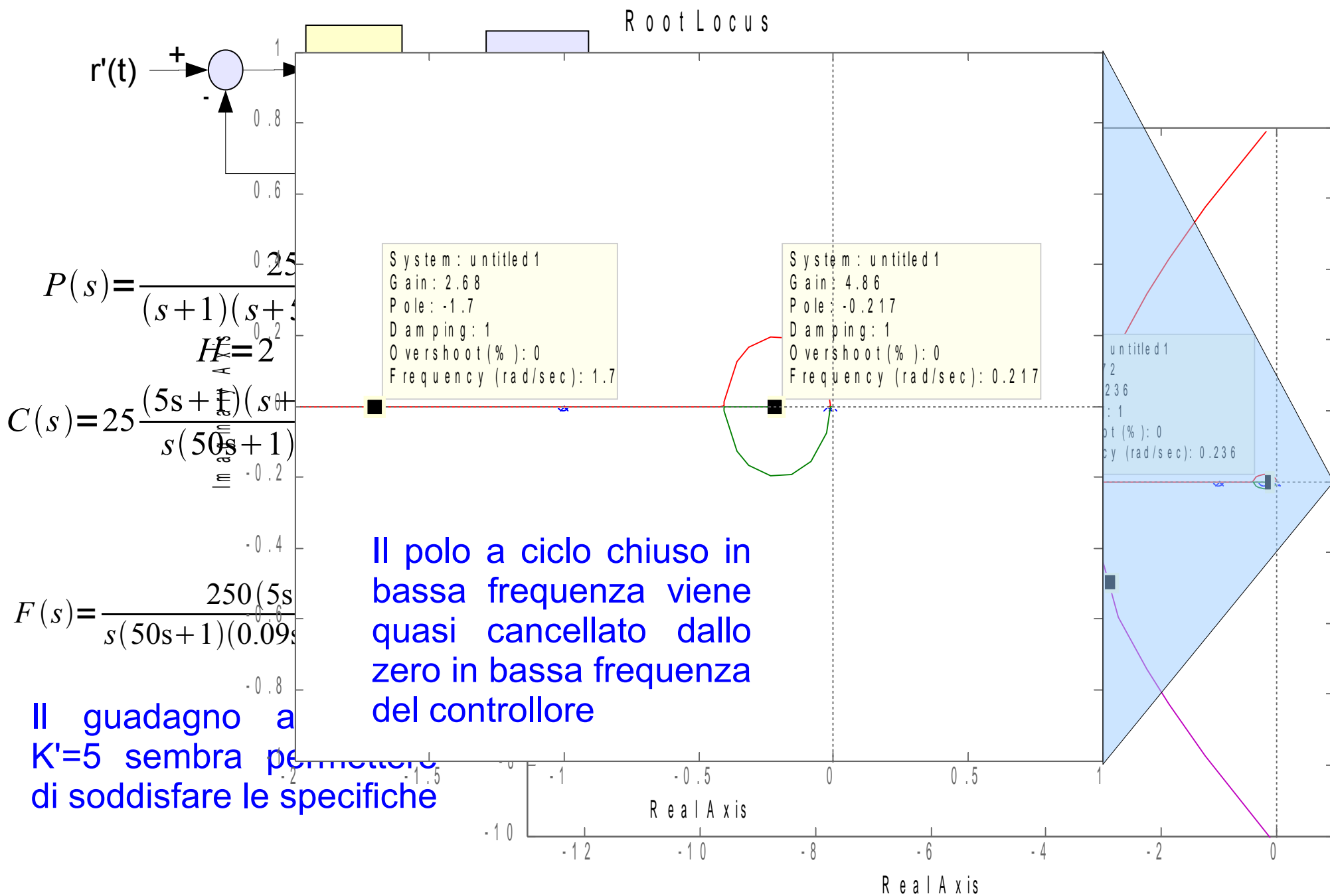
$$C(s) = 25 \frac{(5s+1)(s+1)(0.2s+1)}{s(50s+1)(0.09s+1)}$$

$$F(s) = \frac{250(5s+1)}{s(50s+1)(0.09s+1)(s+10)}$$

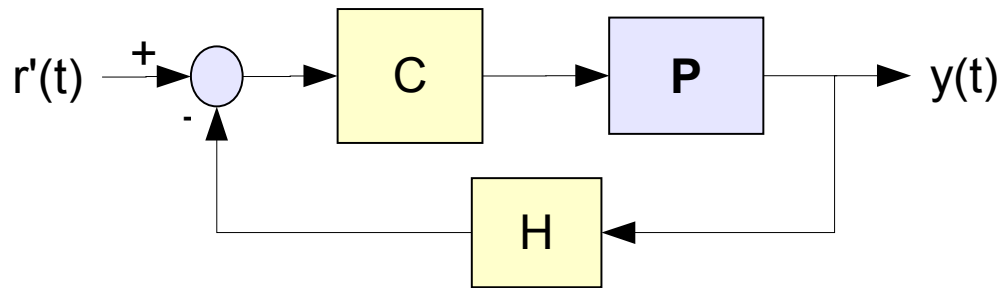
Il guadagno aggiuntivo  $K'=5$  sembra permettere di soddisfare le specifiche



# Esempio



## Esempio



$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}$$

$$H = 2$$

$$C(s) = 25 \frac{(5s+1)(s+1)(0.2s+1)}{s(50s+1)(0.09s+1)}$$

$$F(s) = \frac{250(5s+1)}{s(50s+1)(0.09s+1)(s+10)}$$

```

Command Window
File Edit Debug Desktop Window Help

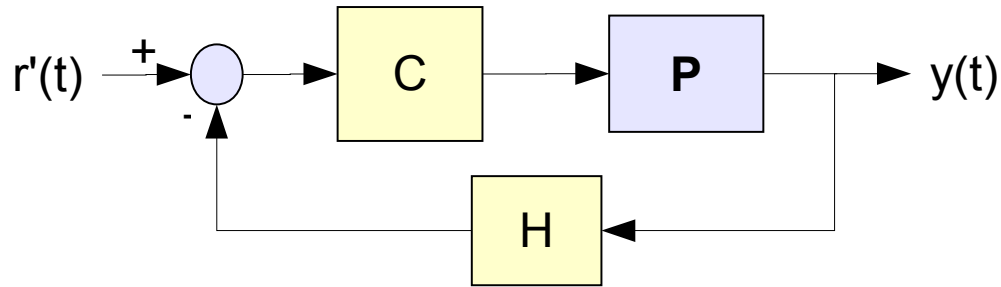
>> P=zpk([],[-1 -5 -10],25)

Zero/pole/gain:
      25
-----
(s+1) (s+5) (s+10)

>> C=tf(5*conv([5 1],conv([1 1],[0.2 1])),conv([50 1],conv([0.09 1],[1 0])))

Transfer function:
      5 s^3 + 31 s^2 + 31 s + 5
-----
      4.5 s^3 + 50.09 s^2 + s
  
```

## Esempio



$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}$$

$$H = 2$$

$$C(s) = 25 \frac{(5s+1)(s+1)(0.2s+1)}{s(50s+1)(0.09s+1)}$$

$$F(s) = \frac{250(5s+1)}{s(50s+1)(0.09s+1)(s+10)}$$

```

Command Window
File Edit Debug Desktop Window Help
>> P=zpk([],[-1 -5 -10],25)

Command Window
File Edit Debug Desktop Window Help
>> C=tf(5*conv([5 1],conv([1 1],[0.2 1])),conv([50 1],conv([0.09 1],[1 0])))

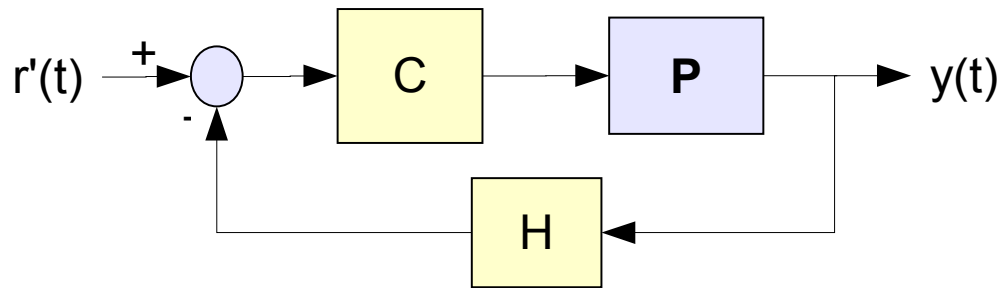
Transfer function:
5 s^3 + 31 s^2 + 31 s + 5
-----
4.5 s^3 + 50.09 s^2 + s

>> H=tf(2,1)

Transfer function:
2

>> rlocus(P*C*H)
fx >>
  
```

# Esempio



$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}$$

$$H = 2$$

$$C(s) = 25 \frac{(5s+1)(s+1)(0.2s+1)}{s(50s+1)(0.09s+1)}$$

$$F(s) = \frac{250(5s+1)}{s(50s+1)(0.09s+1)(s+10)}$$

```

Command Window
File Edit Debug Desktop Window Help
>> P=zpk([],[-1 -5 -10],25)

Command Window
File Edit Debug Desktop Window Help
>> C=tf(5*conv([5 1],conv([1 1],[0.2 1]))/conv([50 1],conv([0.09 1],[1 10])))

Command Window
File Edit Debug Desktop Window Help
>> W=feedback(5*C*P,H)

Zero/pole/gain:
      138.8889 (s+5) (s+1) (s+0.2)
-----
(s+14.89) (s+5) (s+1) (s+0.2163) (s^2 + 6.03s + 17.26)

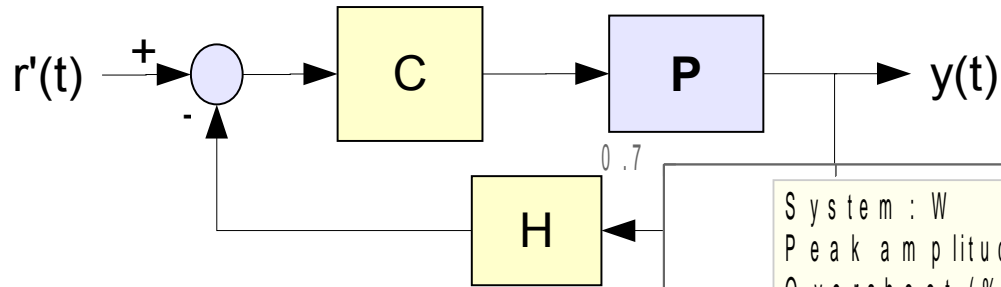
>> step(W)
>> roots([1 6.03 17.26])

ans =

-3.0150 + 2.8583i
-3.0150 - 2.8583i
  
```



# Esempio

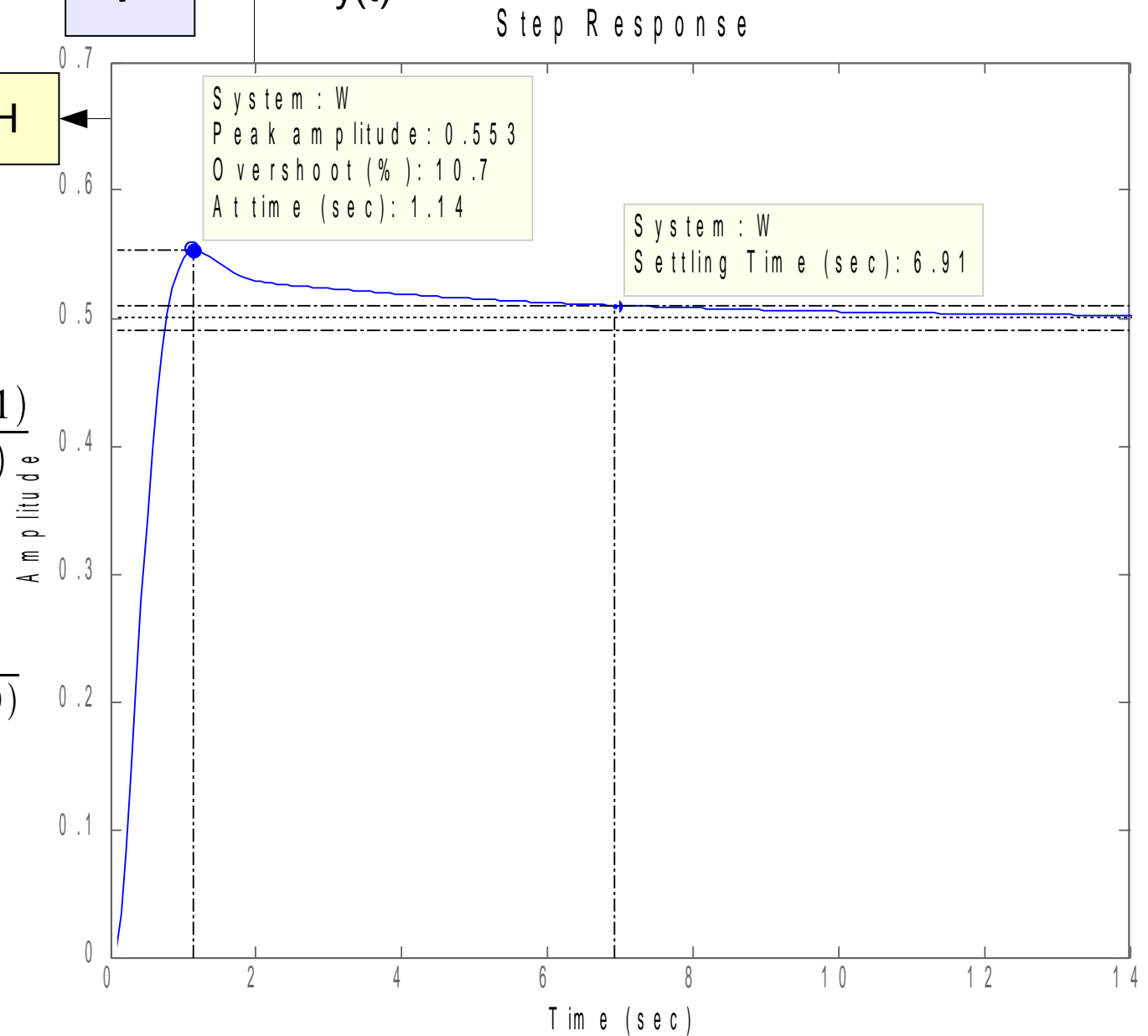


$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}$$

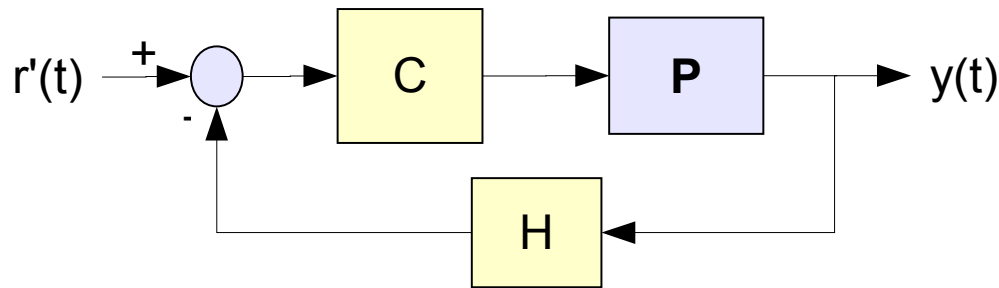
$$H = 2$$

$$C(s) = 25 \frac{(5s+1)(s+1)(0.2s+1)}{s(50s+1)(0.09s+1)}$$

$$F(s) = \frac{250(5s+1)}{s(50s+1)(0.09s+1)(s+10)}$$



## Esempio



$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}$$

$$H = 2$$

$$C(s) = 5 \frac{(25s+1)(s+1)(0.2s+1)}{s(50s+1)(0.09s+1)}$$

$$F(s) = \frac{50(25s+1)}{s(50s+1)(0.09s+1)(s+10)}$$

Avvicinando lo zero della coppia polo-zero all'origine e non incrementando il guadagno del controllore....

```

Command Window
File Edit Debug Desktop Window Help

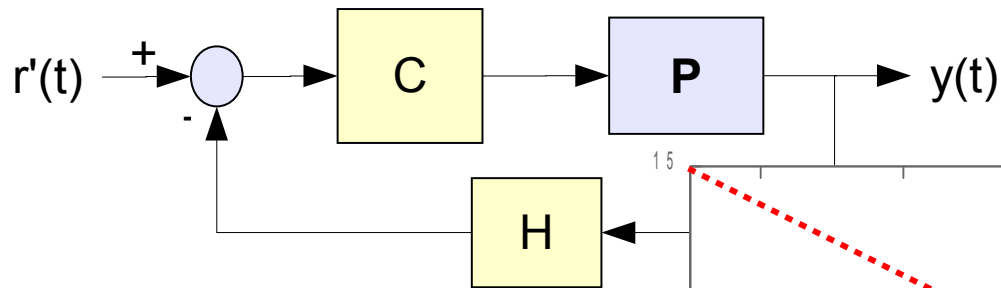
>> C=tf(5*conv([25 1],conv([1 1],[0.2 1])),conv([50 1],conv([0.09 1],[1 0])))

Transfer function:
25 s^3 + 151 s^2 + 131 s + 5
-----
4.5 s^3 + 50.09 s^2 + s

>> rlocus(P*C*H)
>> W=feedback(C*P,H)

Zero/pole/gain:
138.8889 (s+5) (s+1) (s+0.04)
-----
(s+14.91) (s+5) (s+1) (s+0.04033) (s^2 + 6.186s + 18.49)
  
```

# Esempio



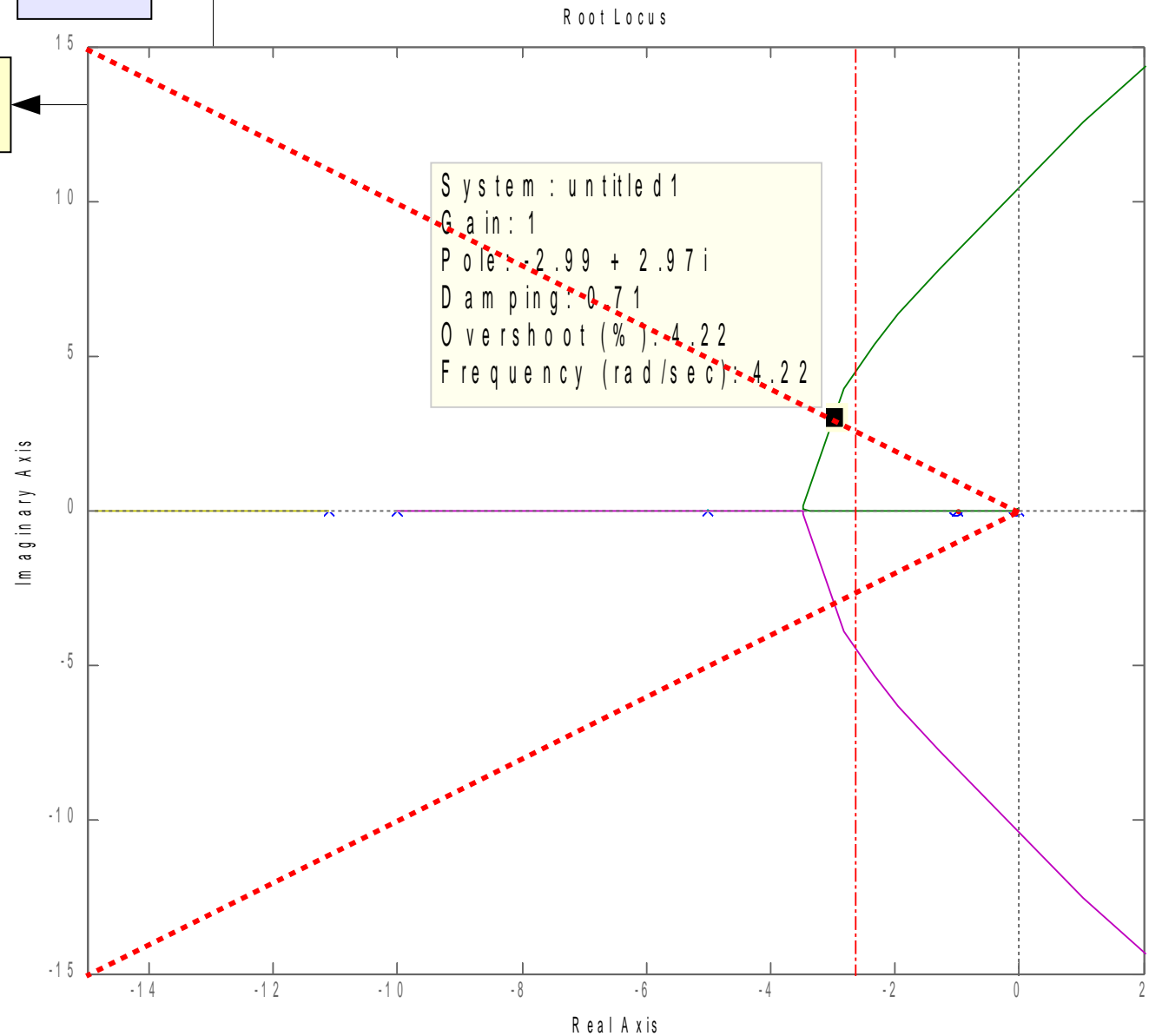
$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}$$

$$H = 2$$

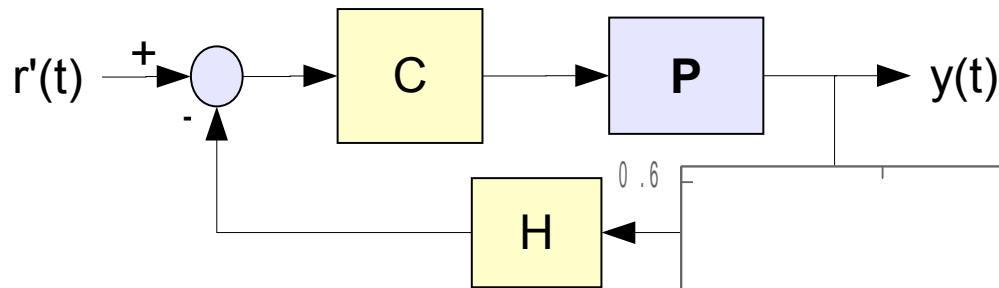
$$C(s) = 5 \frac{(25s+1)(s+1)(0.2s+1)}{s(50s+1)(0.09s+1)}$$

$$F(s) = \frac{50(25s+1)}{s(50s+1)(0.09s+1)(s+10)}$$

Avvicinando lo zero della coppia polo-zero all'origine e non incrementando il guadagno del controllore....



# Esempio



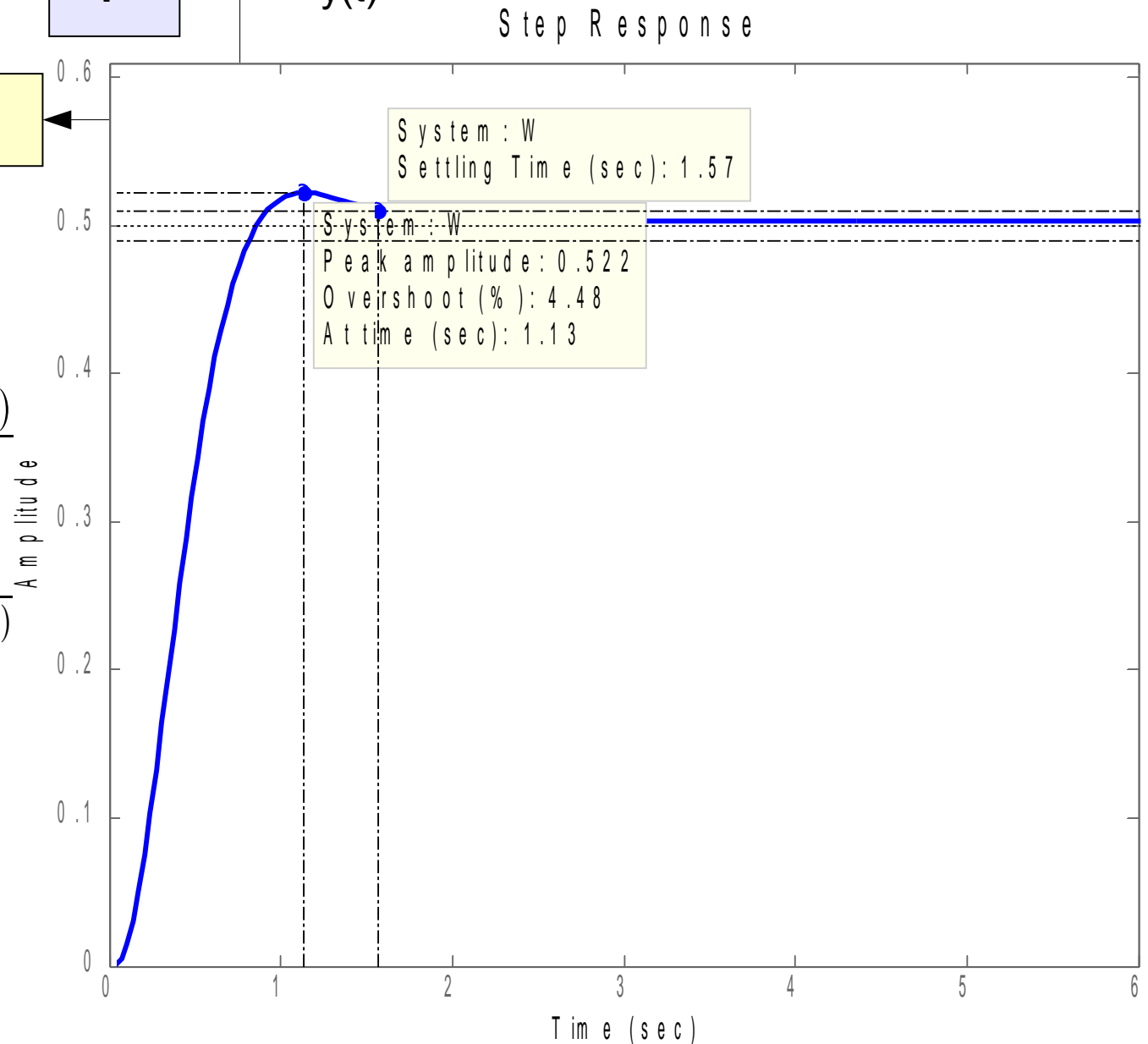
$$P(s) = \frac{25}{(s+1)(s+5)(s+10)}$$

$$H = 2$$

$$C(s) = 5 \frac{(25s+1)(s+1)(0.2s+1)}{s(50s+1)(0.09s+1)}$$

$$F(s) = \frac{50(25s+1)}{s(50s+1)(0.09s+1)(s+10)}$$

Avvicinando lo zero della coppia polo-zero all'origine e non incrementando il guadagno del controllore....



## Riepilogo

- Le specifiche sul comportamento nel transitorio sono state riportate in forma grafica sul piano complesso (di Gauss)
- Sono state presentate i principali effetti della introduzione di poli e zeri a ciclo aperto sul luogo delle radici del polinomio caratteristico a ciclo chiuso
- E stato presentato un esempio di sintesi con l'ausilio del luogo delle radici